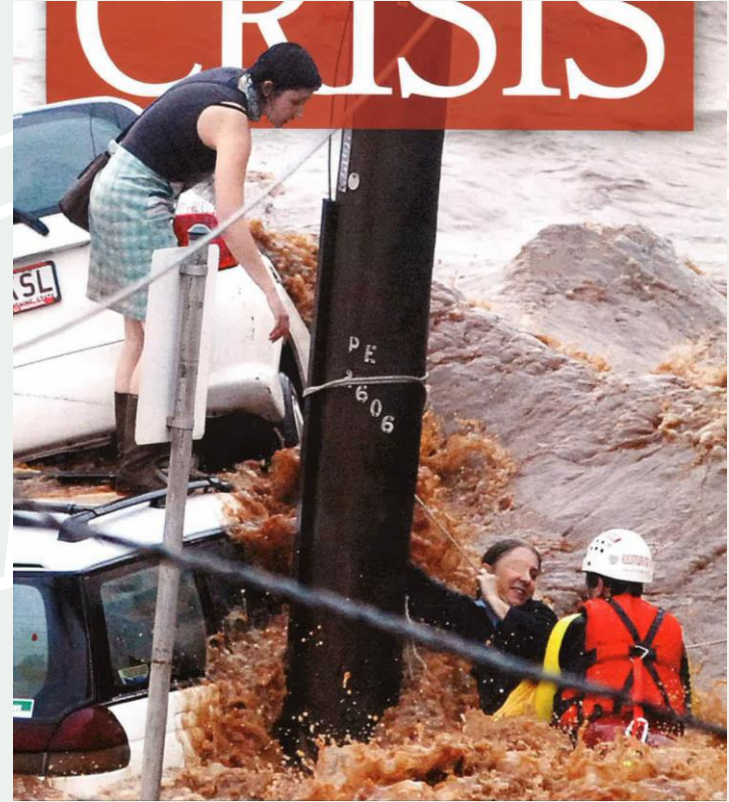


Recent Advancements in 2D Hydraulic Modelling

Water NZ Modelling Symposium

Bill Syme
Senior Principal
BMT



The Toowoomba Chronicle

Overview

A Step-Change in 2D Flood Modelling

Cell Size Independent Turbulence Model

- Model at any scale at any resolution

Sub-Grid Sampling (SGS)

- Rotate regular grid in any direction
- Excellent mesh or cell size convergence

Quadtree Mesh

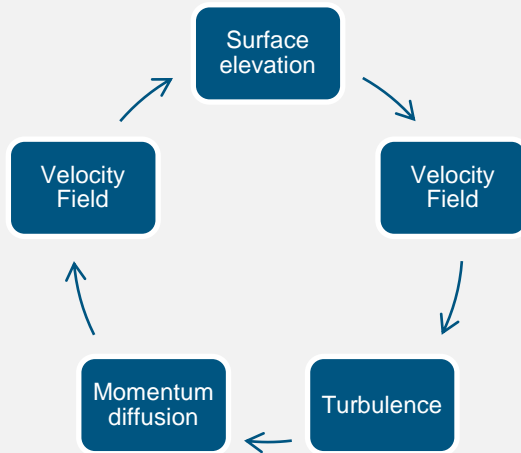
- Very easily vary mesh resolution

Above Combination a Game-Changer!

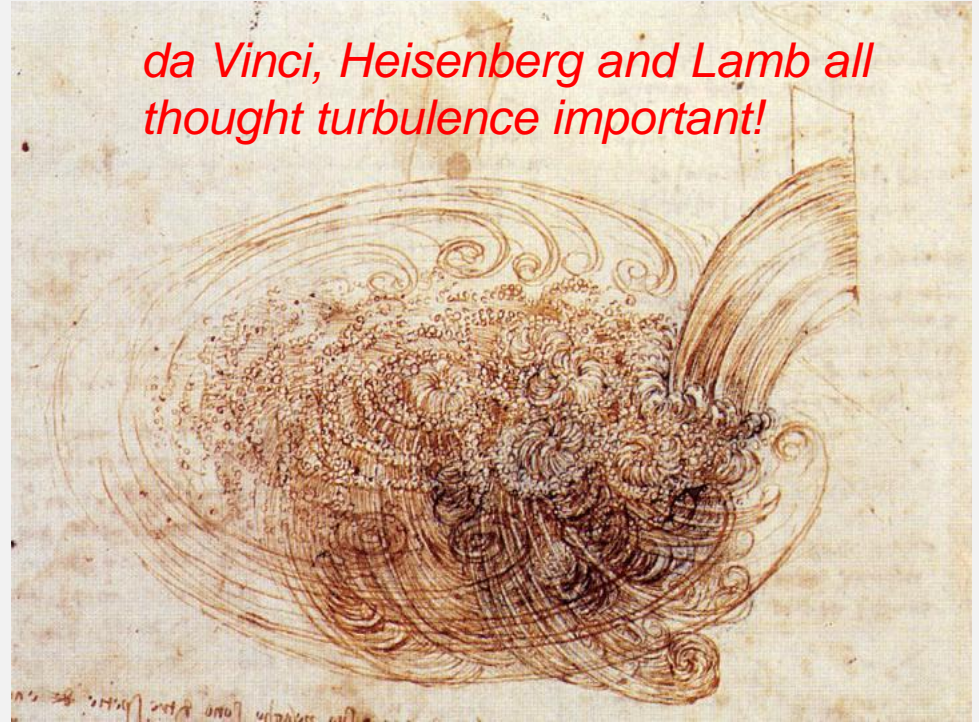
Why Turbulence?

Turbulence causes

- almost infinite flow detail
- momentum diffusivity



da Vinci, Heisenberg and Lamb all thought turbulence important!



Sub-Grid Turbulence

What is “Eddy Viscosity”?

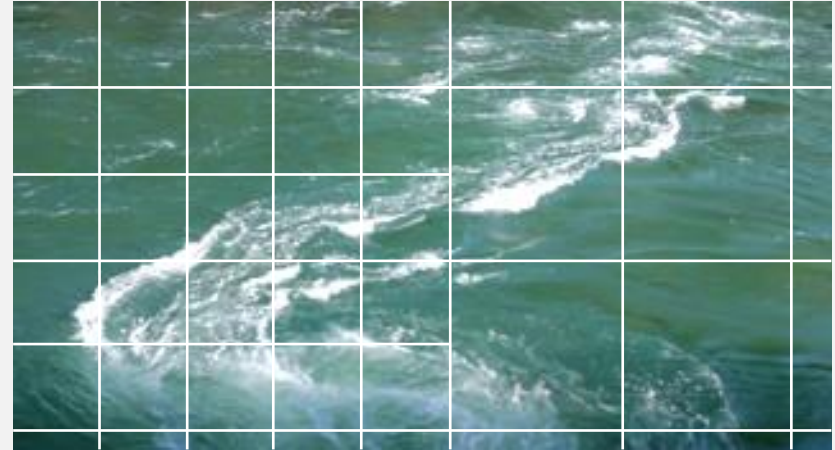
Turbulence in 2D Schemes

- Energy loss due to turbulence within 2D cell
- Traditionally Large Eddy Simulation (LES) approach
 - e.g. Smagorinsky Formulation
 - Good for large cells (relative to the depth)
 - Not designed for when cell size \ll depth

2D Cells

- Becoming smaller and smaller (cell size \ll depth)
- Irregular and Quadtree meshes vary cell size (which ideally use same turbulence parameters)

Need a 2D cell size independent turbulence model

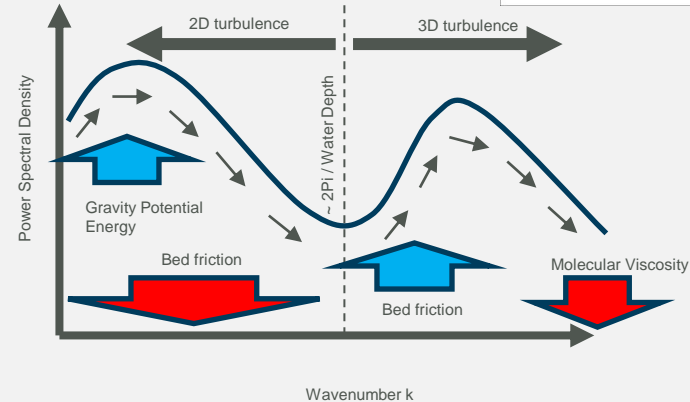
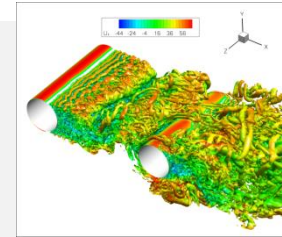
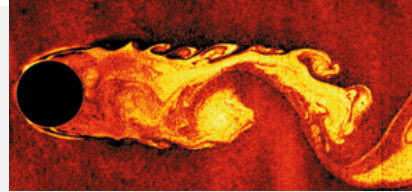


Turbulence in Shallow Fluid Flows

In shallow fluid flows we have both 2D and 3D flow behaviour

Bed friction converts larger scale 2D turbulence into smaller scale 3D turbulence

Need to represent and transition from 2D turbulence (LES) to 3D turbulence



Nadaoka, K., and Yagi, H. (1998). Shallow Water Turbulence Modelling and Horizontal Large Eddy Computation of River Flow. *J. Hydraulic Engineering*, pages 493–500.

Cell Size Independent Sub-Grid Turbulence Approach

Testing of a range of turbulence models

- Constant, Smagorinsky, Wu, Prandtl, k-omega, k-epsilon

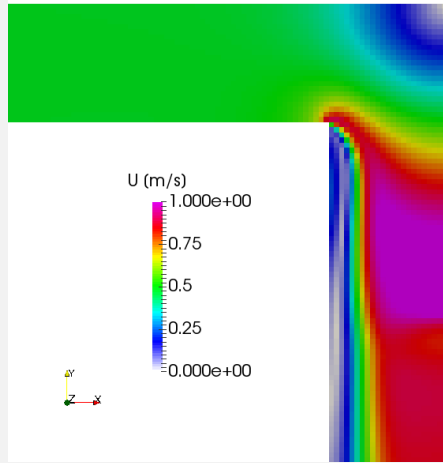
Benchmark to a range of physical scales and range of cell sizes

- Flume Tests
- Real-World: Low data and boundary uncertainties and high quality calibration data
- Determine optimum turbulence model parameters for each scenario

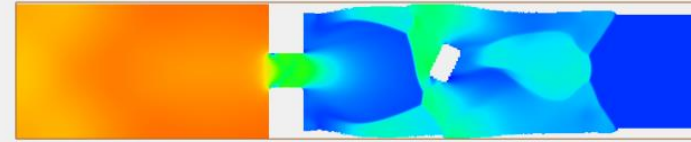
Objective

- A 'one size fits all' turbulence model?

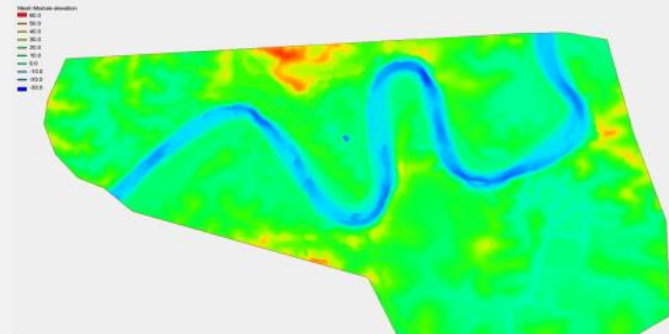
Sub-Grid Turbulence Modelling Benchmark Cases



Right angled flume bend,
Scale 0.15 m width



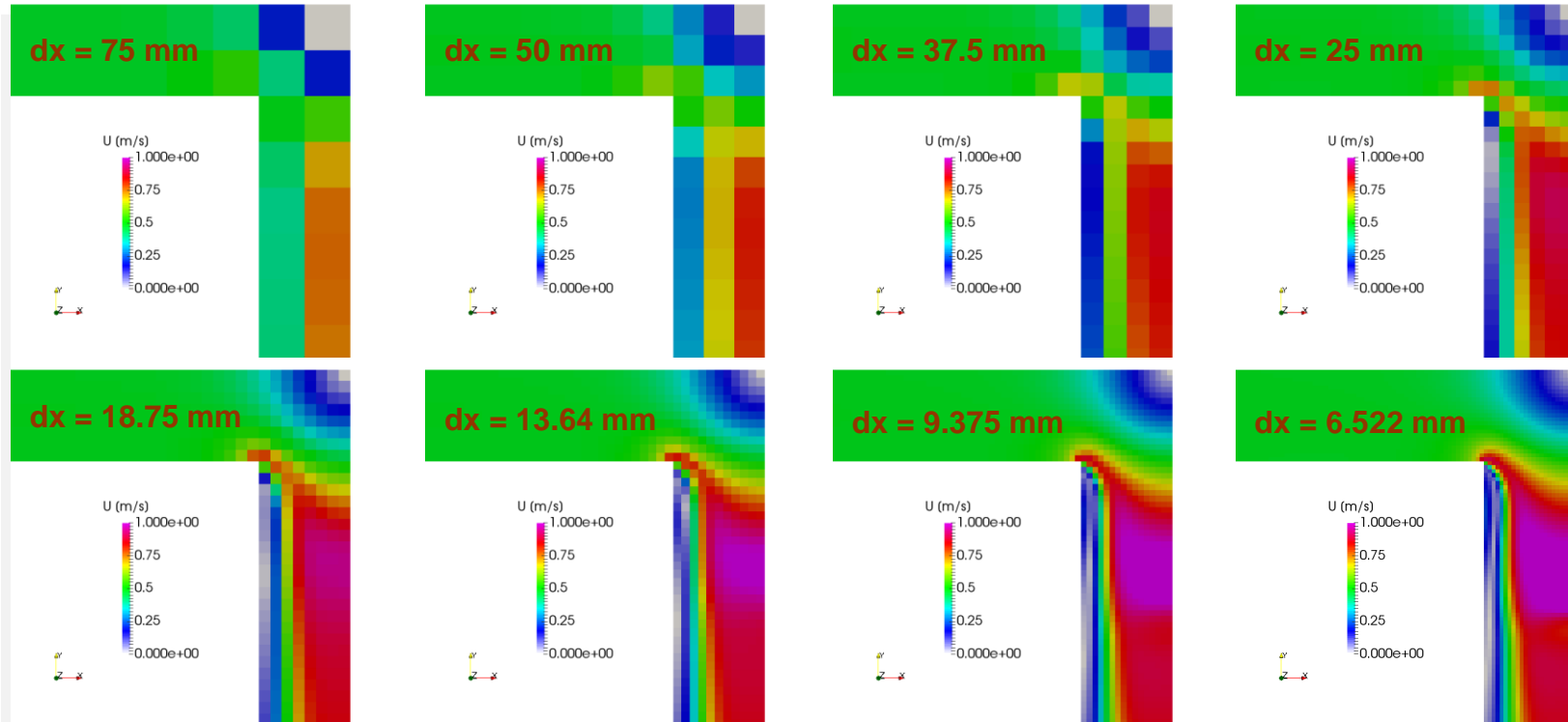
UK EA T06, Scale 3 m width



Brisbane River 2011 flood event, Scale 200 m

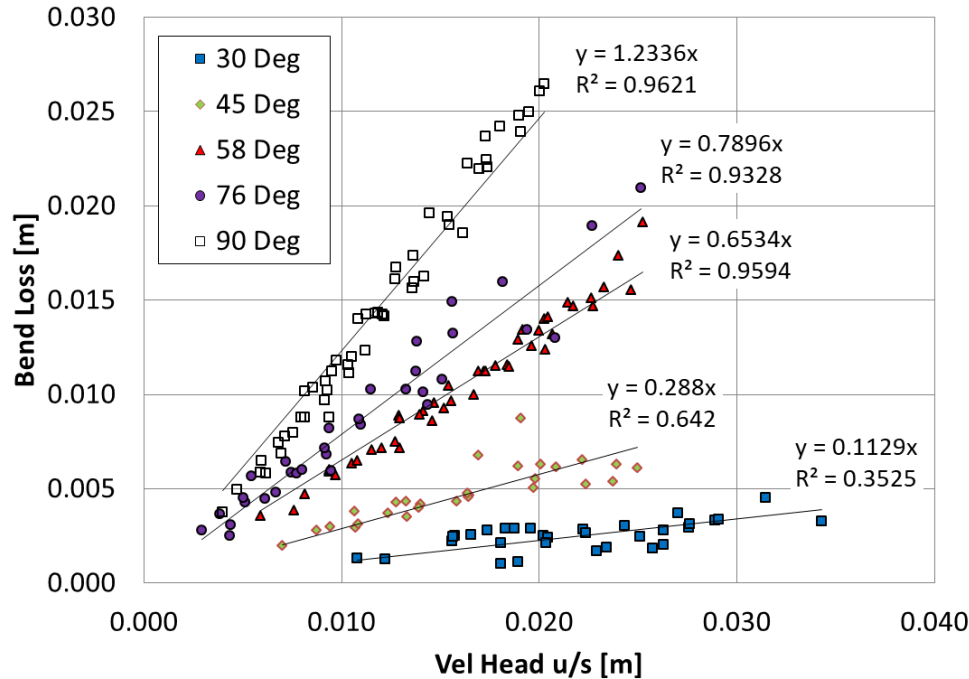
Sub-Grid Turbulence Modelling

Kansas Uni Right Angled Flume Test



Sub-Grid Turbulence Modelling

Kansas Uni flume test bend results



- Malone, T, Parr, D. (2008). Bend Losses in Rectangular Culverts, Kansas Department of Transport (http://ntl.bts.gov/lib/30000/30900/30935/KU-05-5_Final_Report.pdf)
- Excellent correlation between head loss and upstream velocity head
- 90° bend loss factor of 1.22 to 1.42

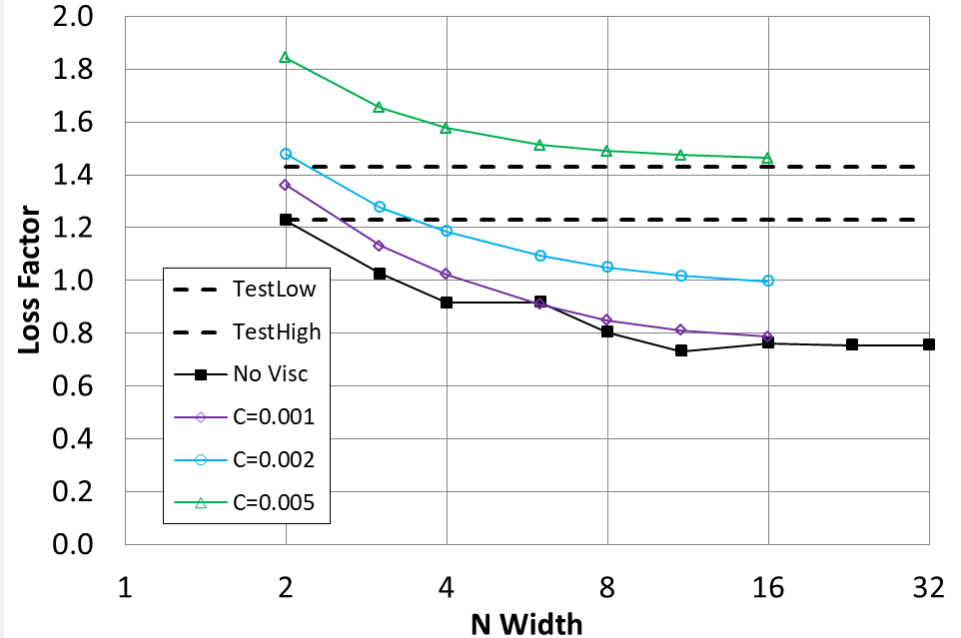
Sub-Grid Turbulence Modelling

90° Bend – Head Loss vs Cell Size

Cell size convergence test

Optimum constant viscosity

- $C = 0.004$ to $0.005 \text{ m}^2/\text{s}$

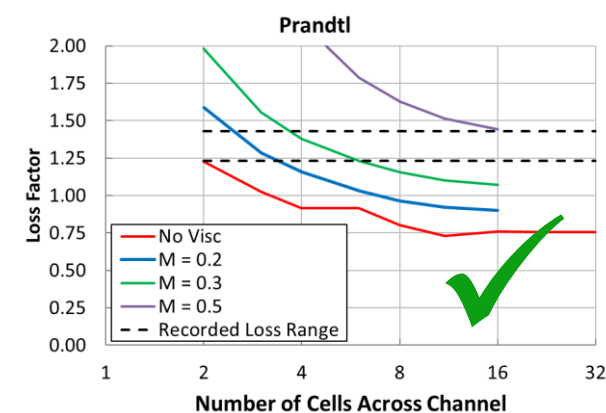
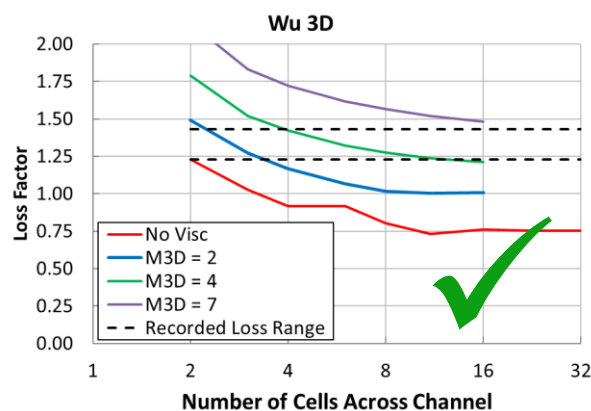
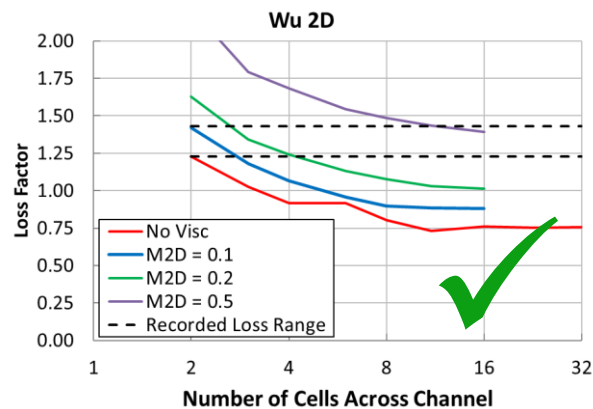
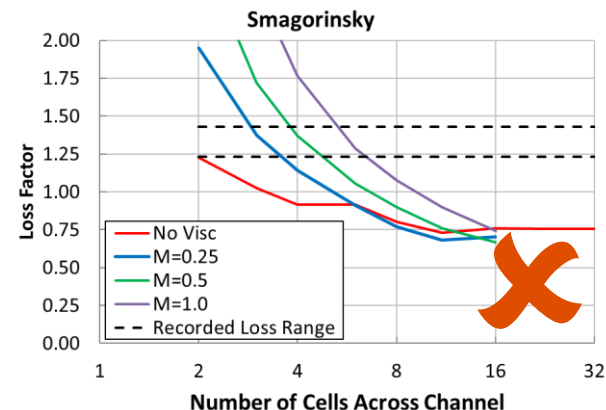
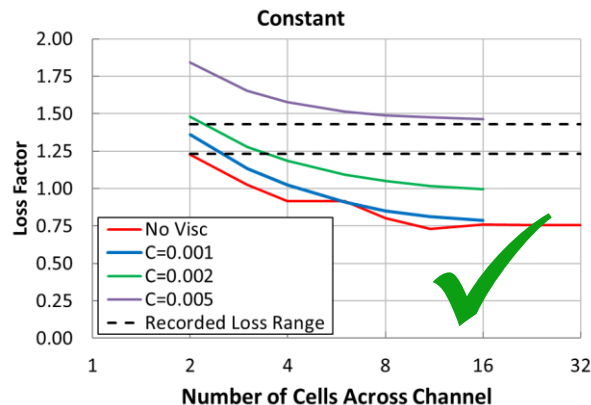
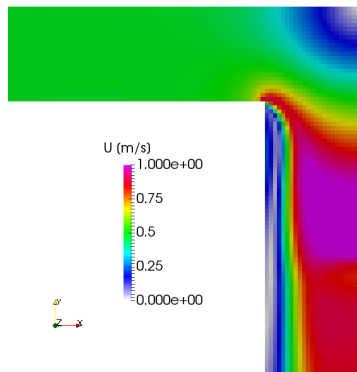


Sub-Grid Turbulence Modelling Sesame Street Game



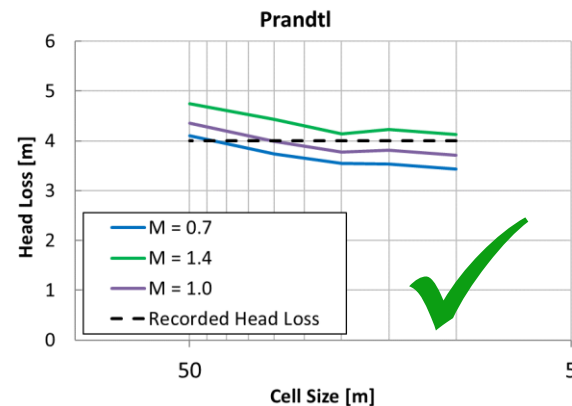
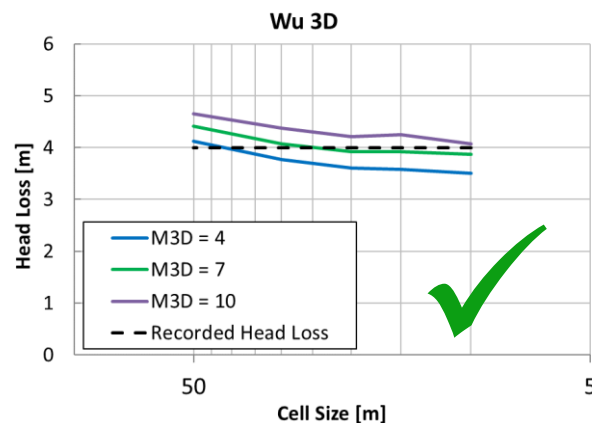
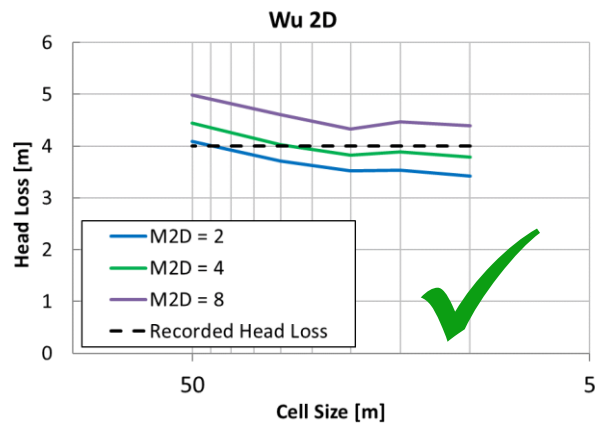
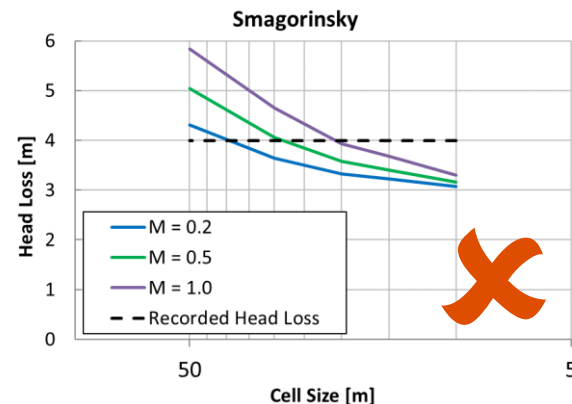
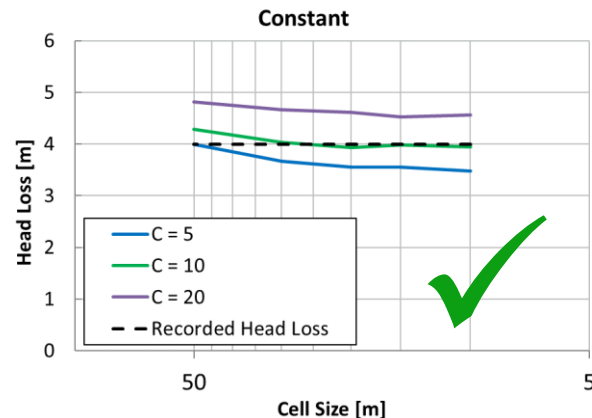
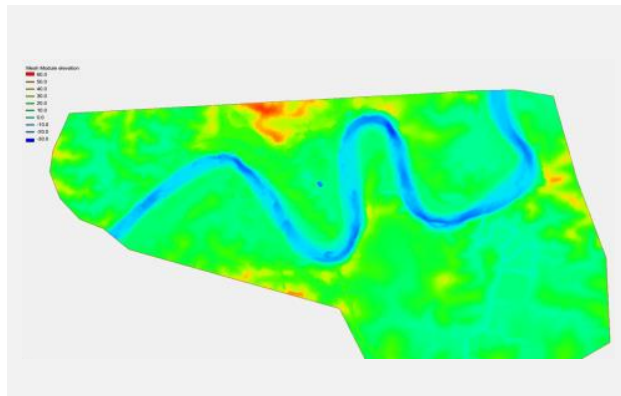
Sub-Grid Turbulence Modelling

90° Bend – Head Loss vs Cell Size



Sub-Grid Turbulence Modelling

Brisbane River – Head Loss vs Cell Size



Sub-Grid Turbulence Modelling

Optimum Parameters Comparison

Case	Smagorinsky	Constant	Wu 2D	Wu 3D	Prandtl
90 Deg Bend (0.15 m)	No optimum	0.004	0.5	6	0.4
Dambreak Flume (3 m)	No optimum	0.01	0.5	3	0.5
Brisbane River (200 m)	No optimum	10	4	7	1.0



Not an option



Impractical
(Very strongly cell
size dependent)



OK
(Some cell size
dependency)



Excellent
outcome



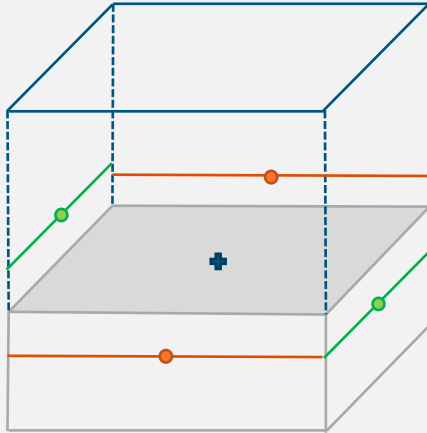
Good
(computationally
and memory
intensive)

Sub-Grid Sampling (SGS)

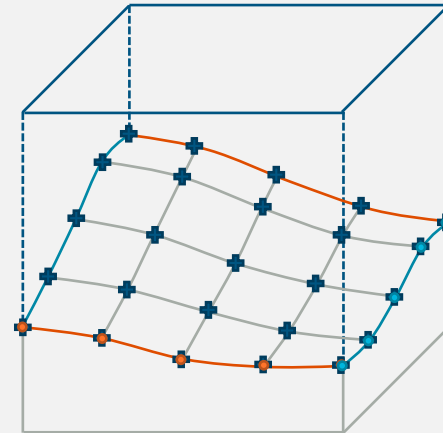
Why?

To make better use of terrain information within a 2D cell

Without SGS
(Conventional Approach)



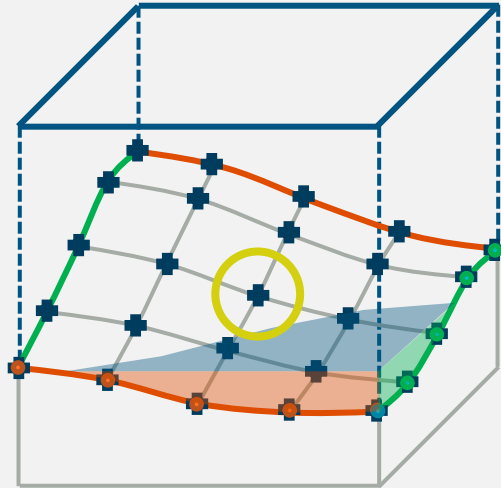
With SGS



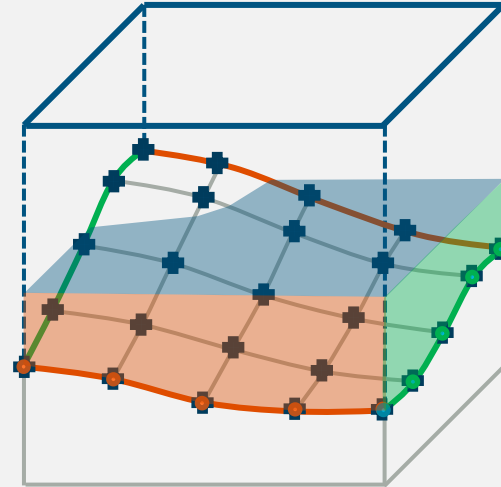
Sub-Grid Sampling (SGS)

Improved Conveyance and Storage

Without SGS cell would be dry at this water level
as cell center is above water level



With SGS cell 25% partially wet.
Two cell faces flowing.



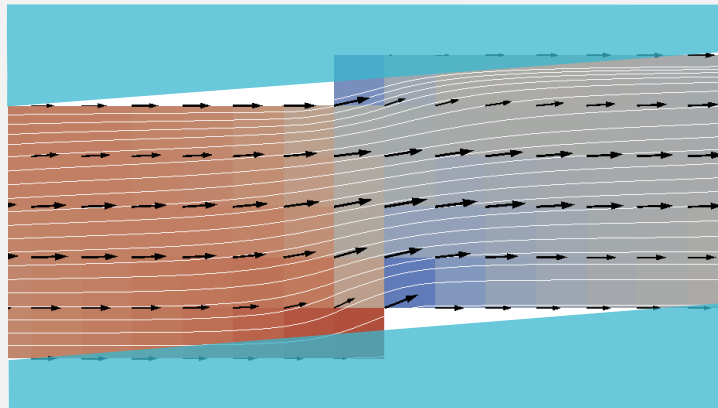
Cell 85% partially wet.
Four cell faces flowing.

SGS Benchmarking

Deep Sided Channels Unaligned to Grid

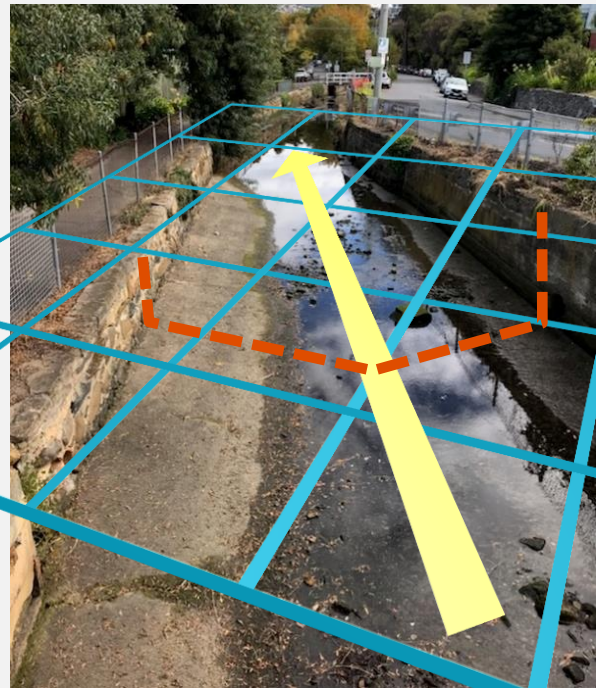
Mesh not aligned with deep banks (e.g. concrete drains)

- Distorts streamlines
- Artificial energy losses; steepens gradient



Traditional Solutions

- 1D channel with cross-section (time-consuming; full 2D solution compromised)
- Irregular mesh (quadrilaterals aligned with banks)
- Much finer regular mesh (much longer run times)

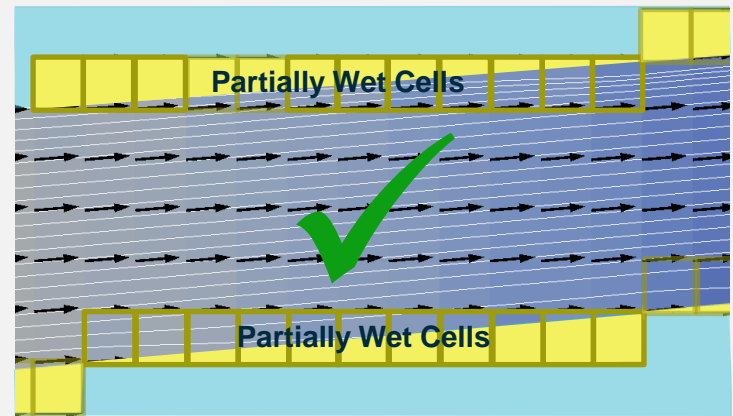
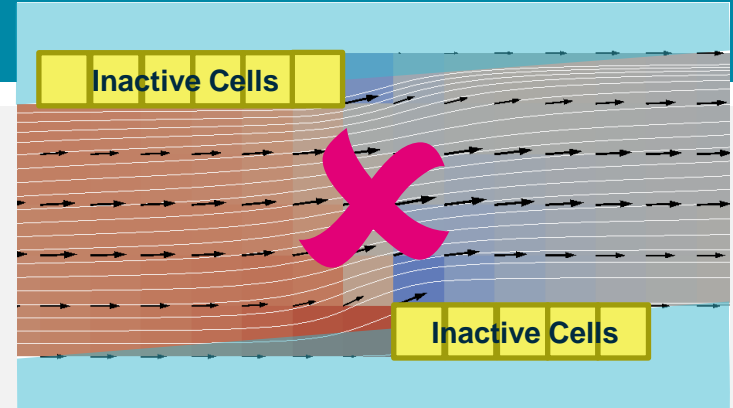


SGS Benchmarking

Deep Sided Channels Unaligned to Grid

Let's try SGS...

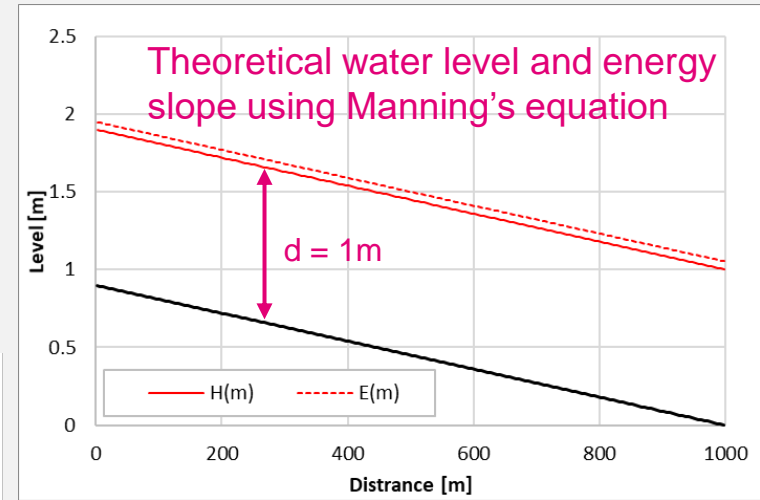
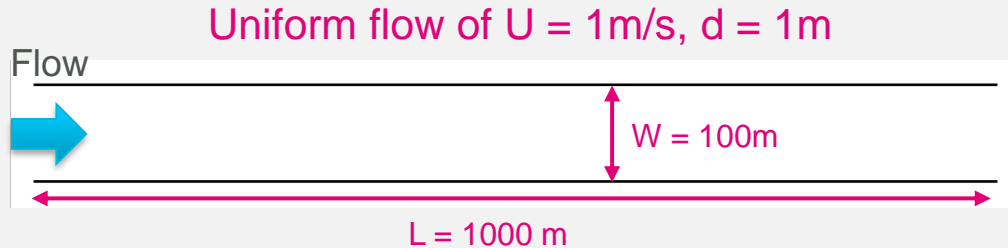
- Cells and cell faces along edge partially wet
- Streamlines parallel with banks 😊
- No apparent artificial energy losses 😊



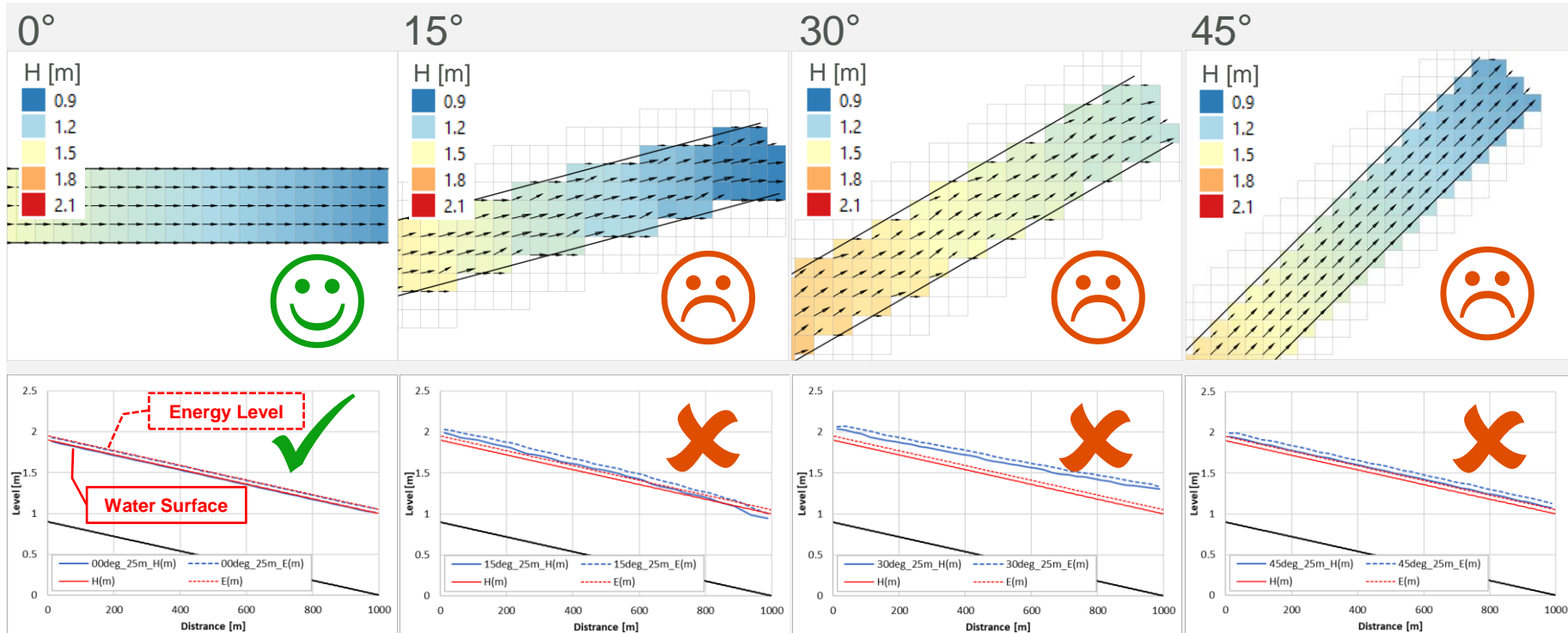
SGS Benchmarking – Manning's Equation

Rectangular Channel Test

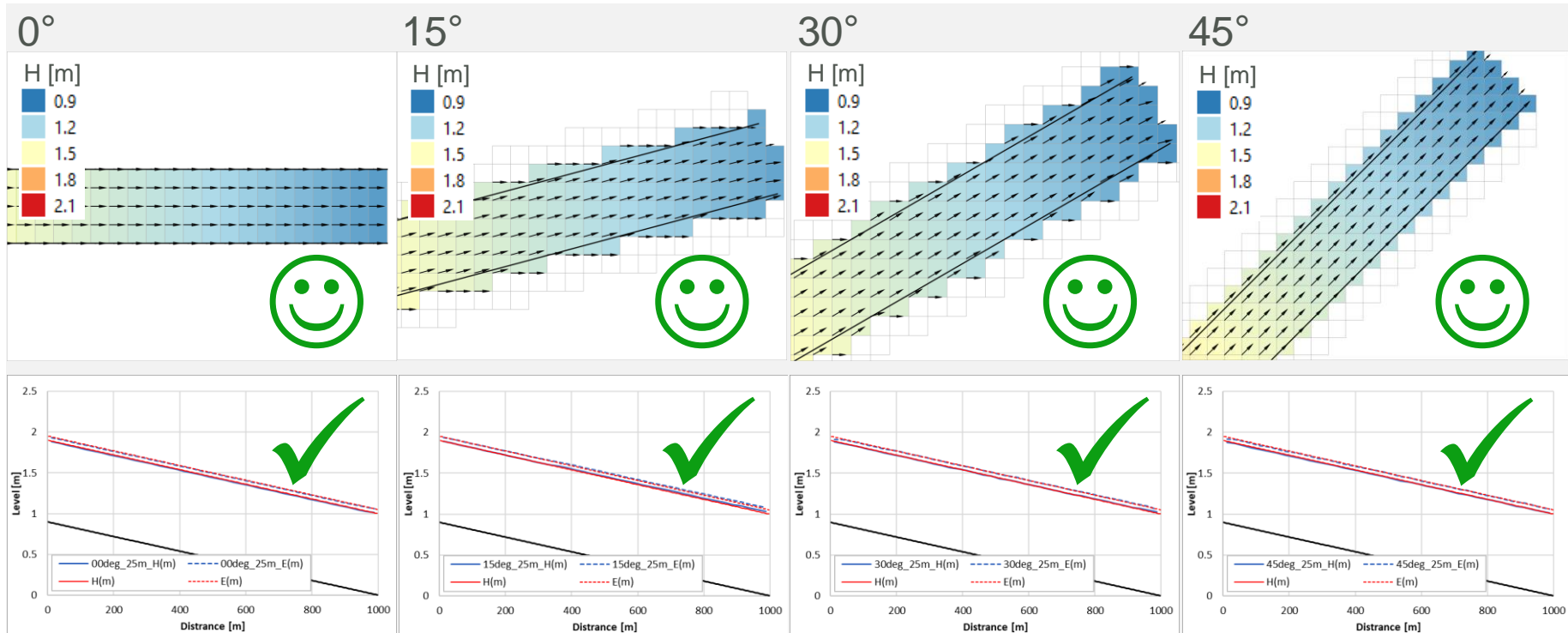
- Rectangular channel with length of 1000m and width of 100m
- Flow rate = 100 m³/s
- Depth = 1 m
- Slope = 0.0009
- Manning's $n = 0.03$



SGS Benchmarking – Manning's Equation Rotated Channel Test – Without SGS



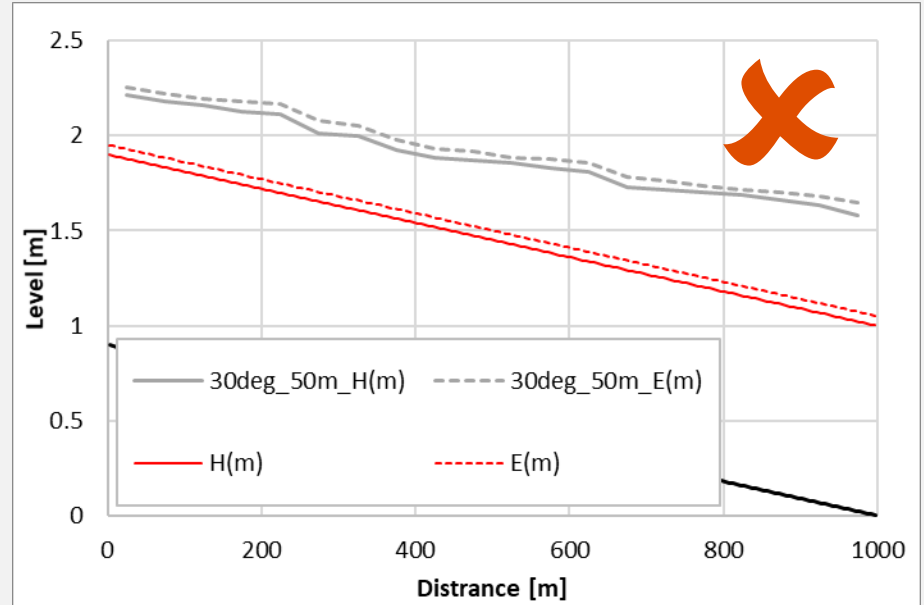
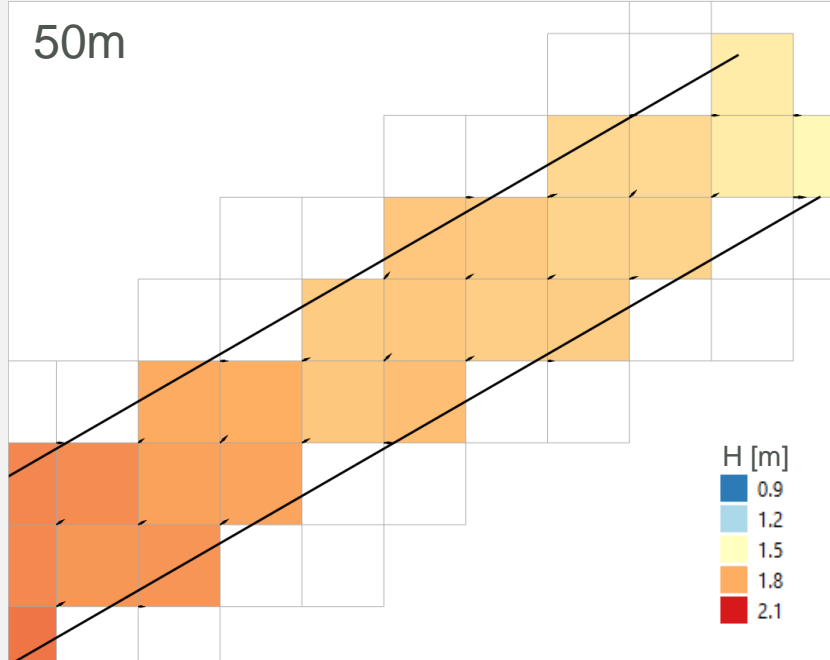
SGS Benchmarking – Manning's Equation Rotated Channel Test – With SGS



SGS Benchmarking – Manning's Equation

Cell Size Sensitivity – Without SGS

TUFLOW HPC – Without SGS

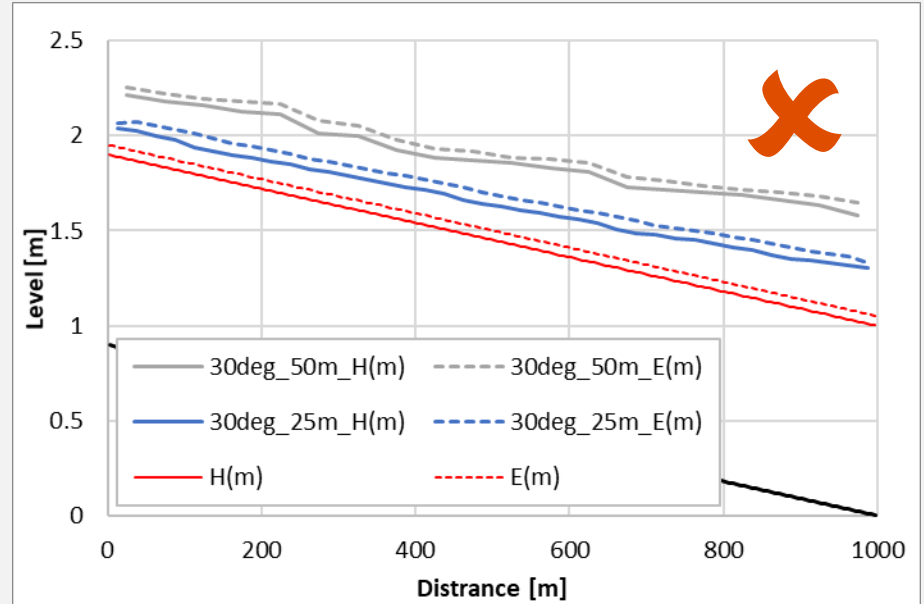
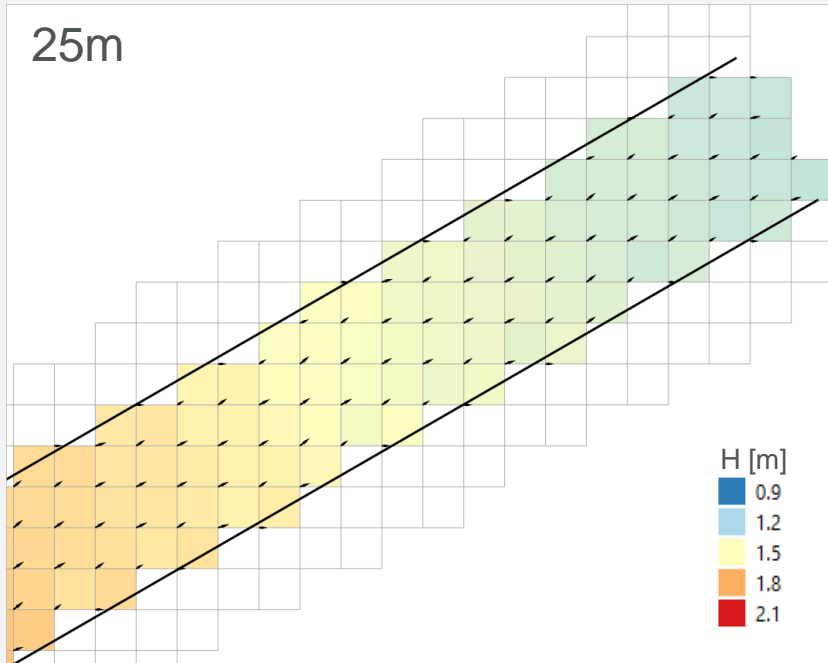


SGS Benchmarking – Manning's Equation

Cell Size Sensitivity – Without SGS

TUFLOW HPC – Without SGS

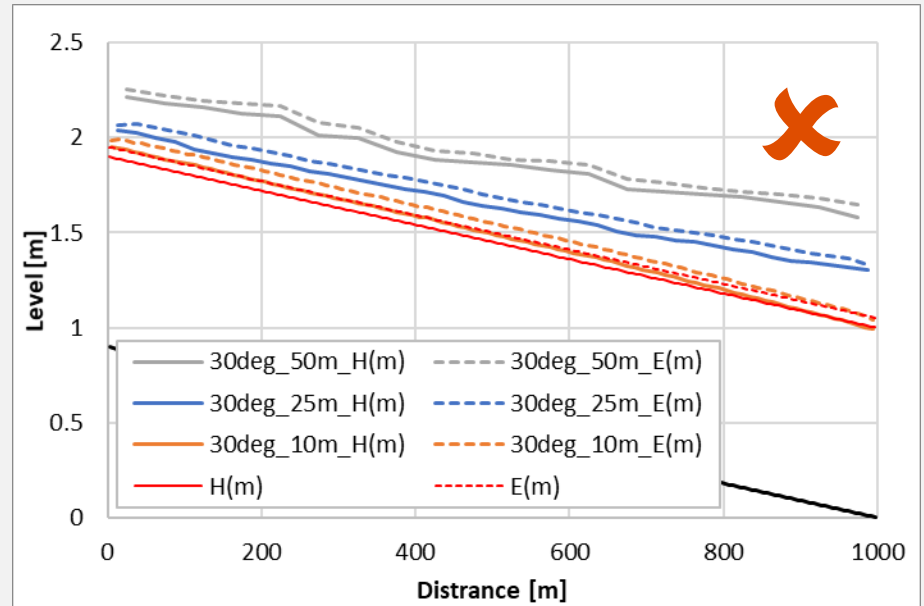
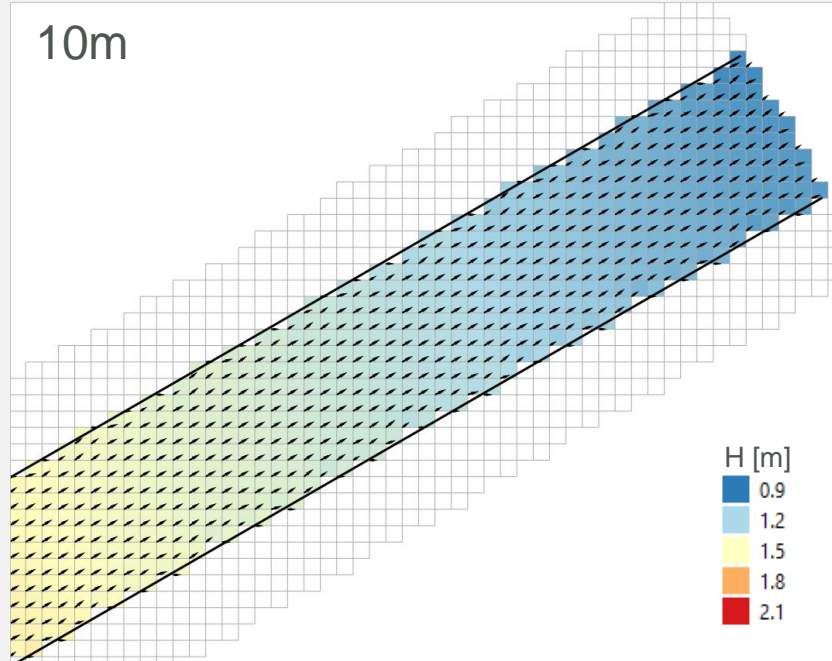
25m



SGS Benchmarking – Manning's Equation

Cell Size Sensitivity – Without SGS

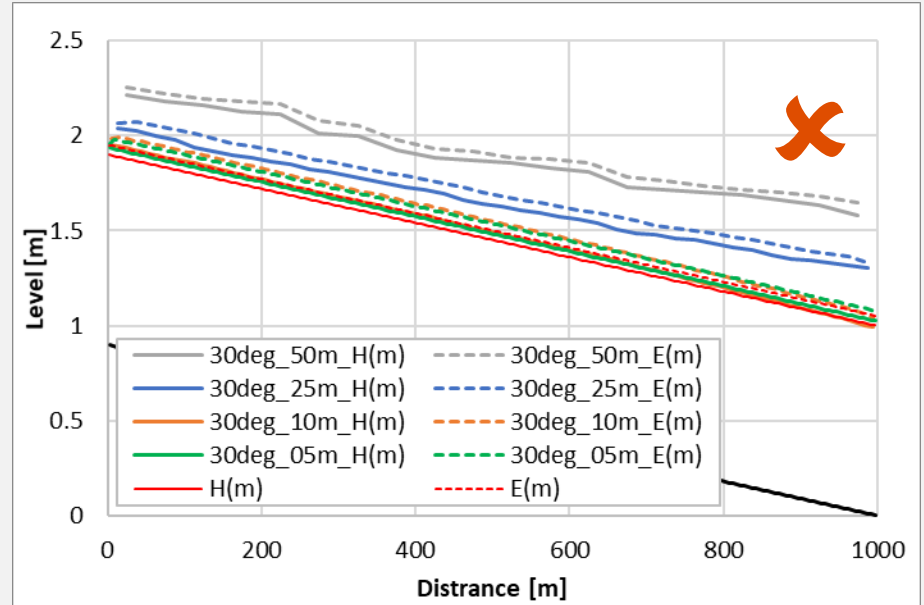
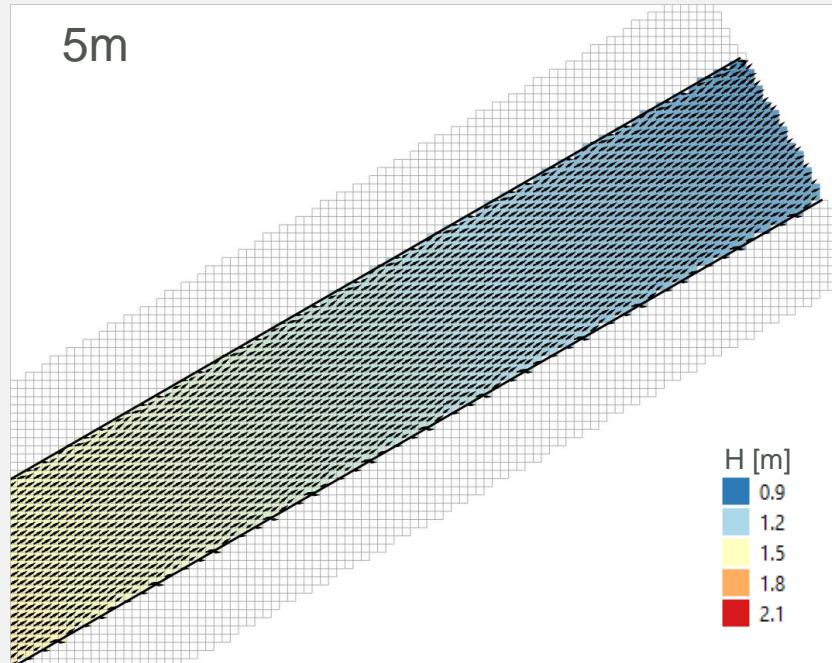
TUFLOW HPC – Without SGS



SGS Benchmarking – Manning's Equation

Cell Size Sensitivity – Without SGS

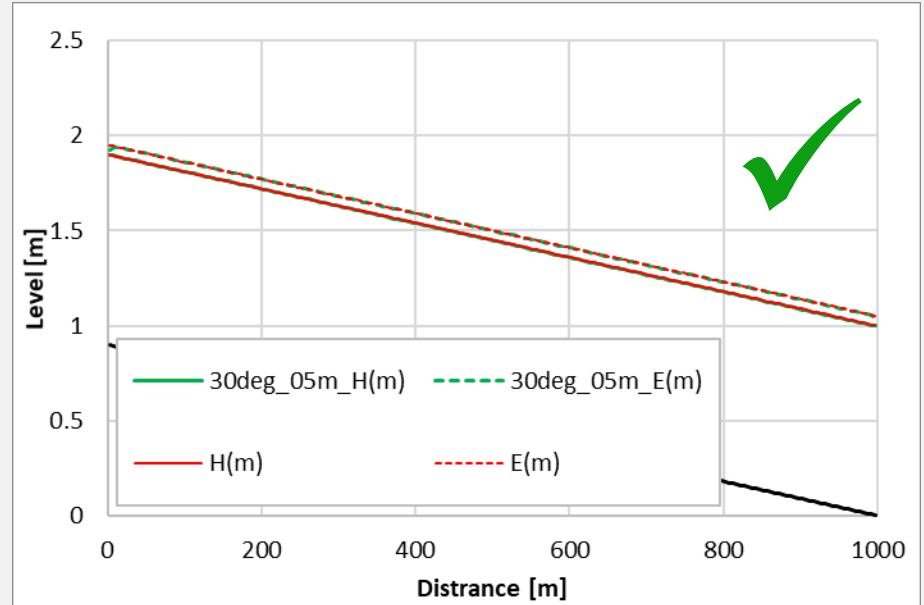
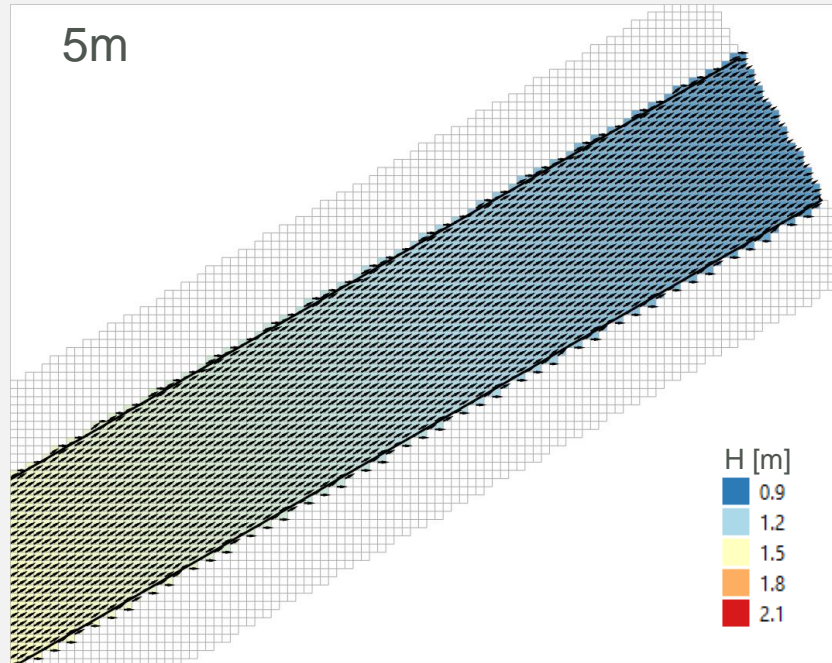
TUFLOW HPC – Without SGS



SGS Benchmarking – Manning's Equation

Cell Size Sensitivity – With SGS

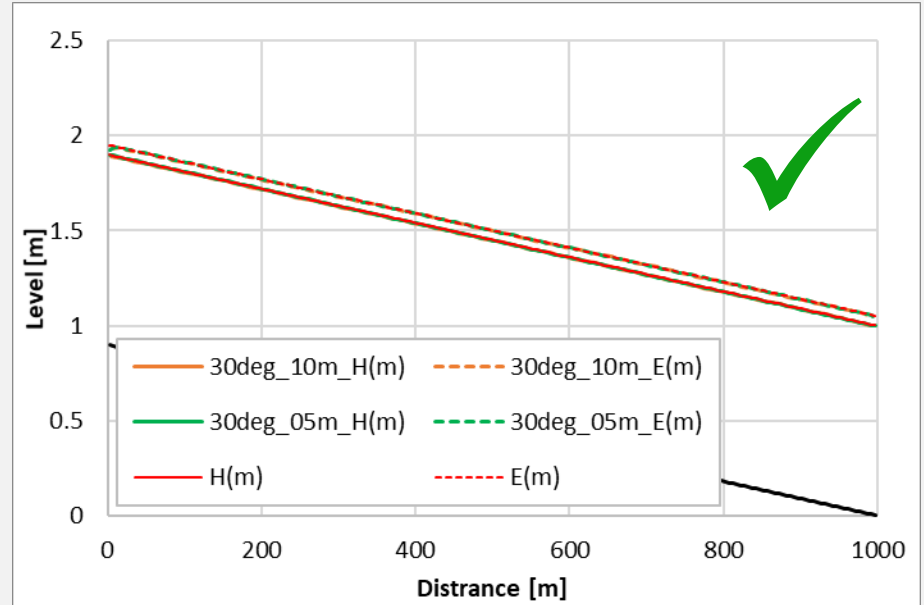
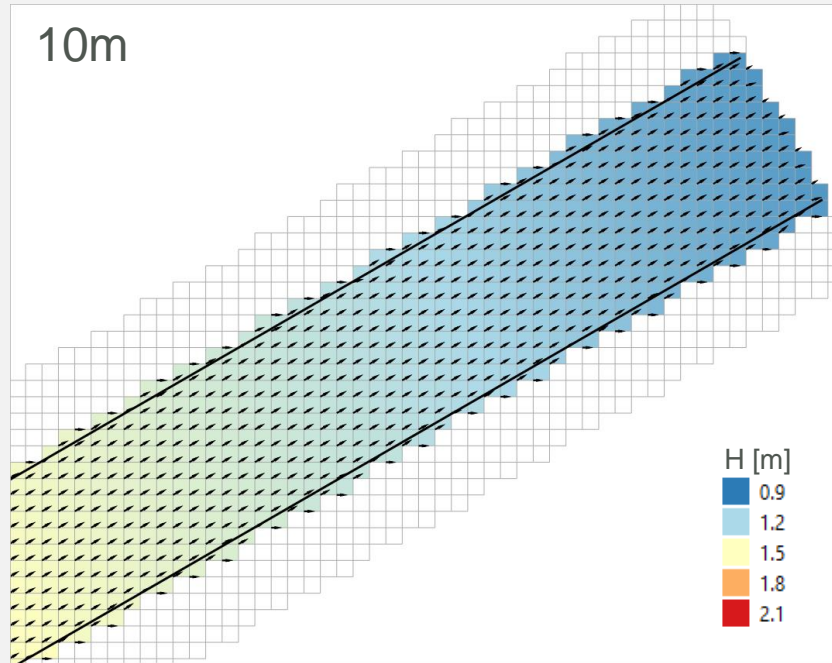
TUFLOW HPC – With SGS



SGS Benchmarking – Manning's Equation

Cell Size Sensitivity – With SGS

TUFLOW HPC – With SGS

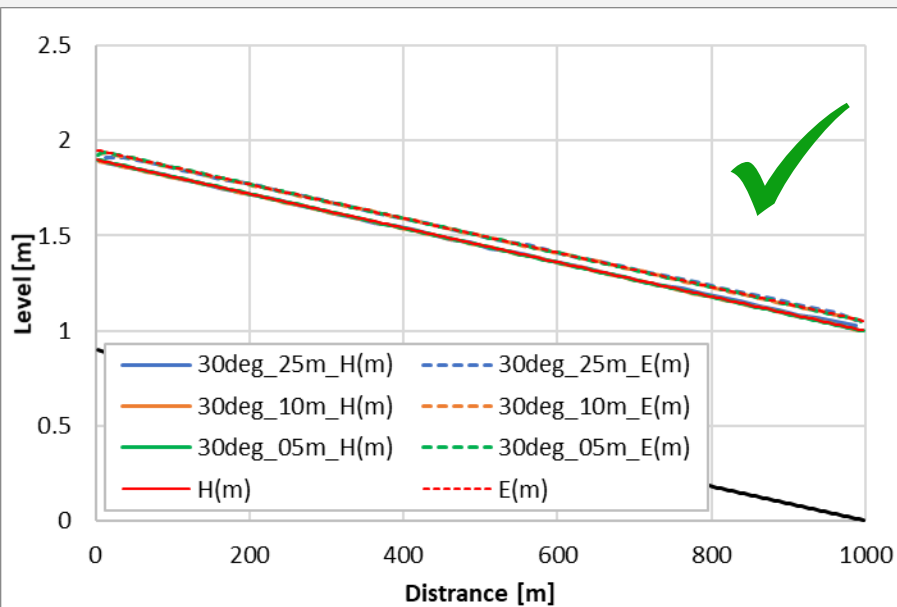
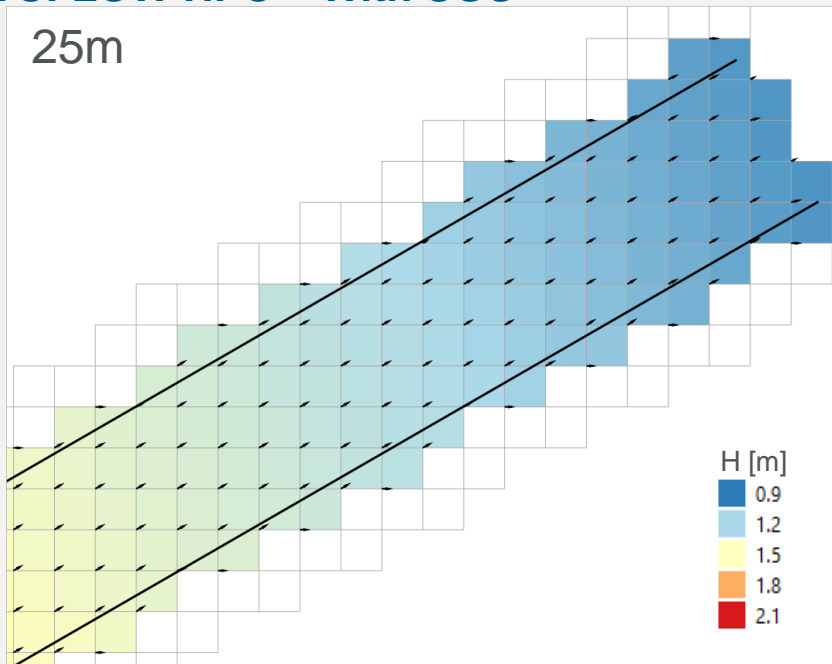


SGS Benchmarking – Manning's Equation

Cell Size Sensitivity – With SGS

TUFLOW HPC – With SGS

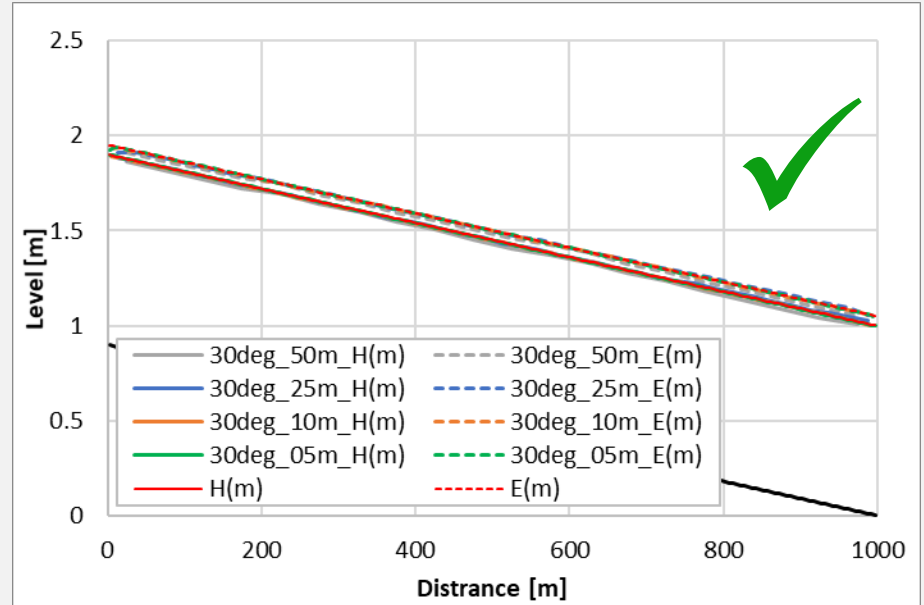
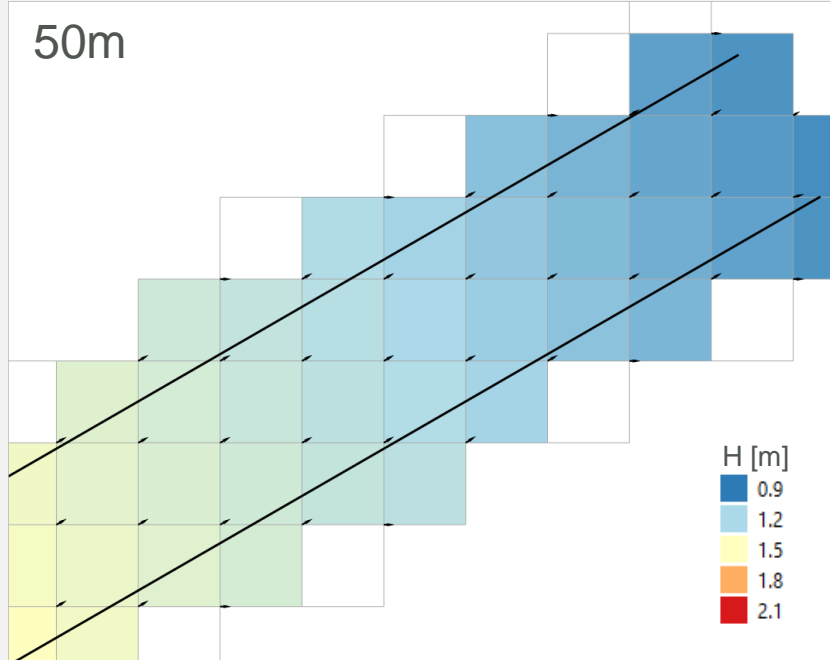
25m



SGS Benchmarking – Manning's Equation

Cell Size Sensitivity – With SGS

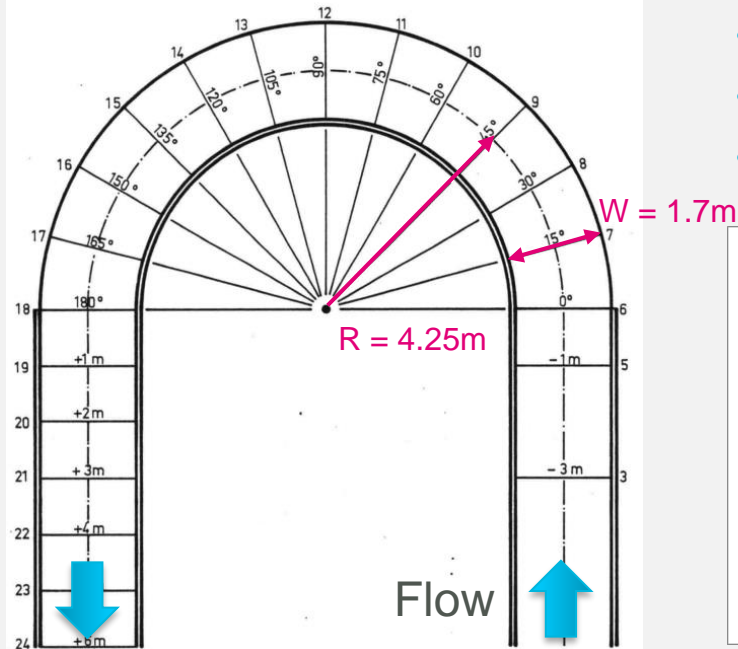
TUFLOW HPC – With SGS



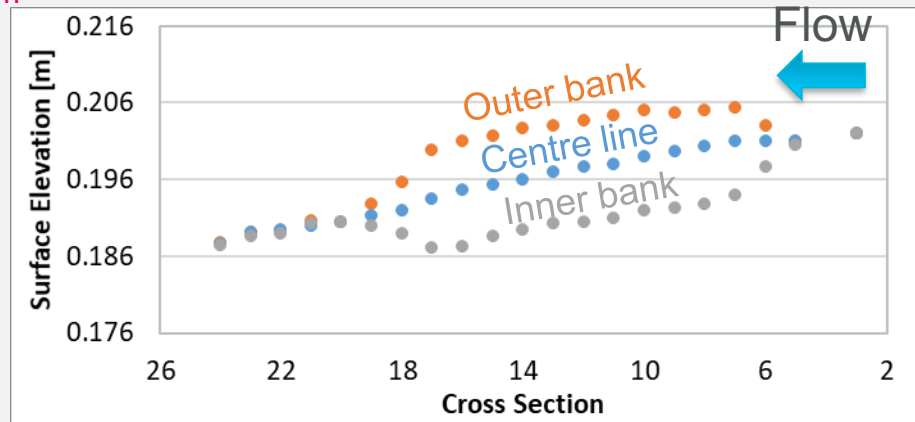
SGS Benchmarking

U-Bend Flume Test – Experiment Set-up

- Flume experiment conducted by De Vriend (1978)



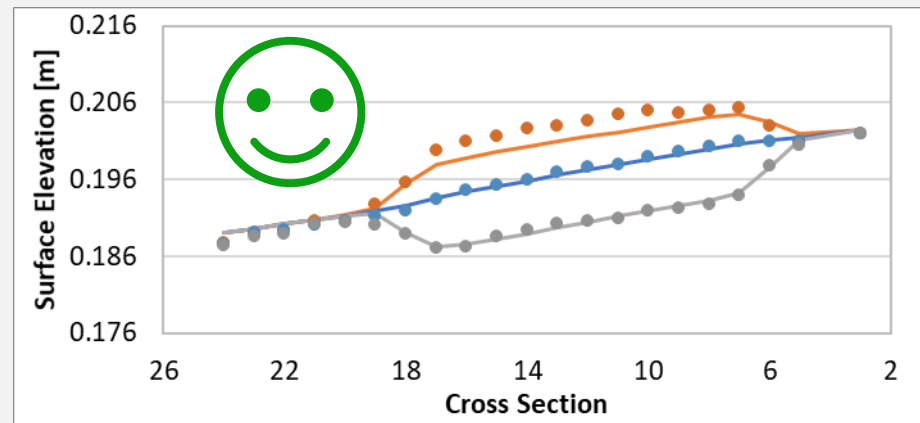
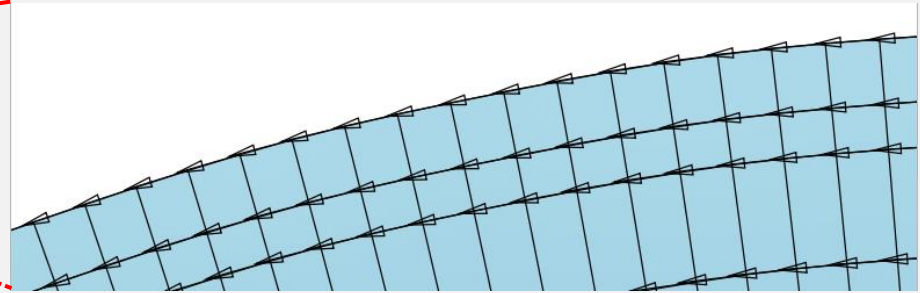
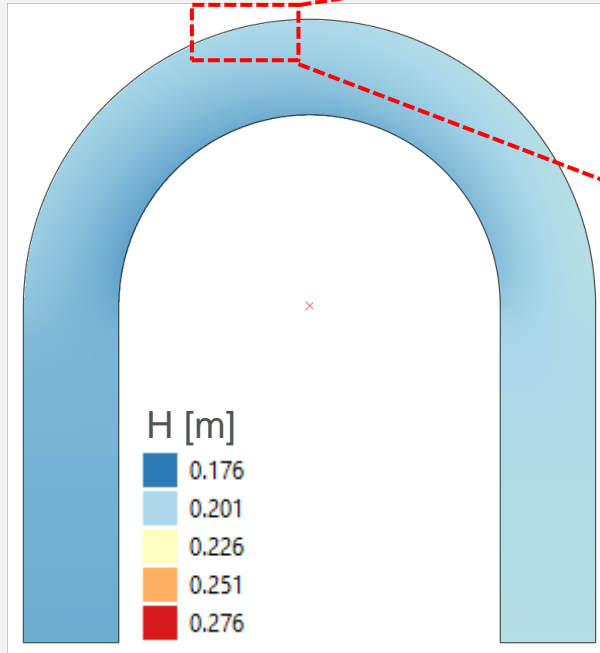
- Flow rate = $0.189\text{ m}^3/\text{s}$
- Downstream $H = 0.18\text{ m}$
- Manning's n estimated to be $0.0115 \sim 0.0125$



SGS Benchmarking

U-Bend Flume Test – Irregular Mesh

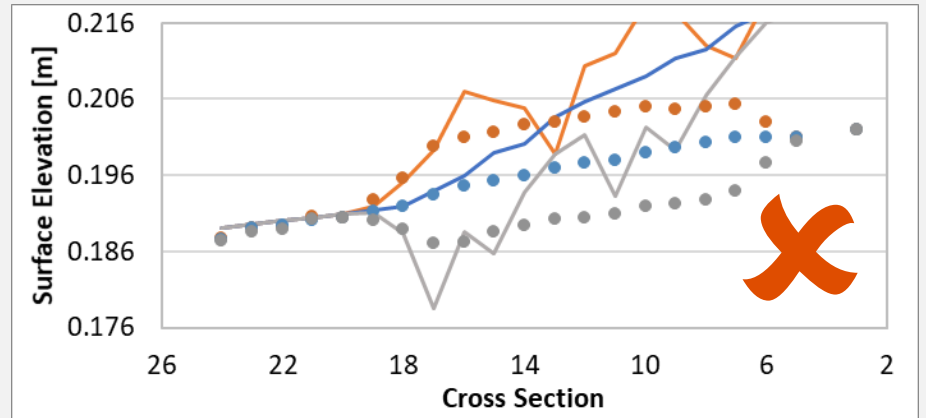
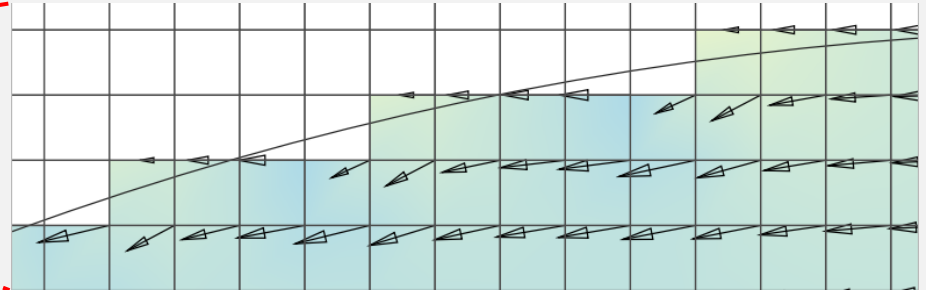
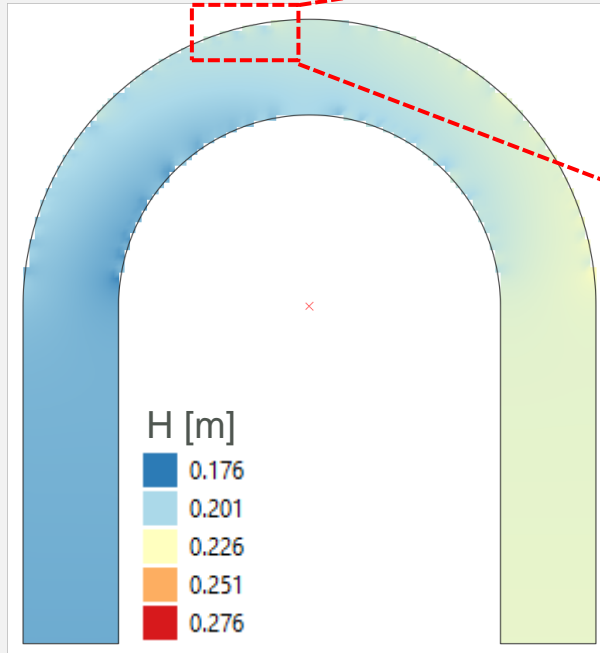
TUFLOW FV



SGS Benchmarking

U-Bend Flume Test – Regular Mesh Without SGS

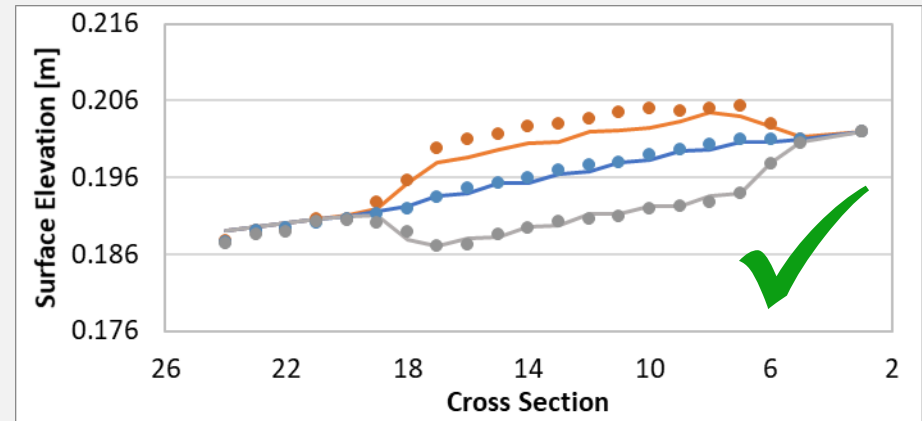
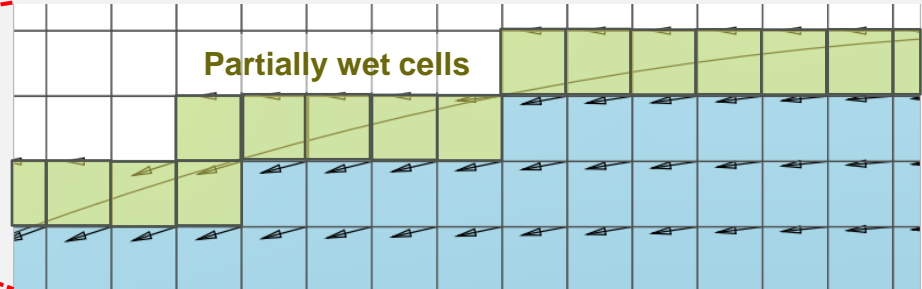
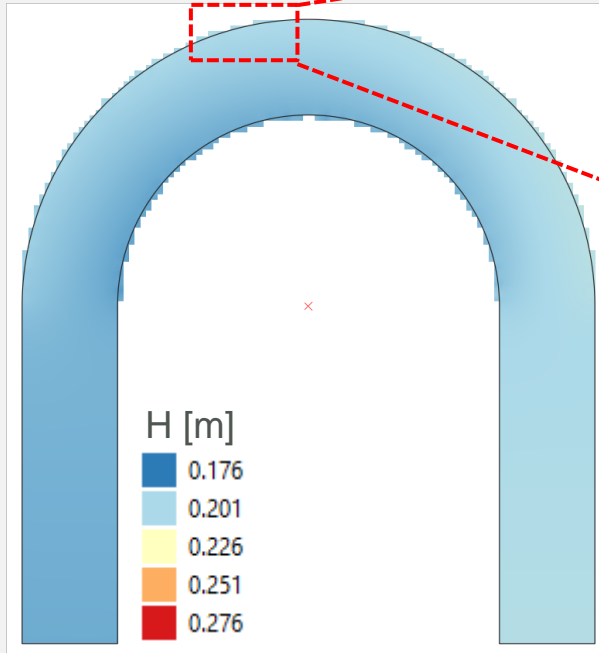
TUFLOW HPC without SGS



SGS Benchmarking

U-Bend Flume Test – Regular Mesh With SGS

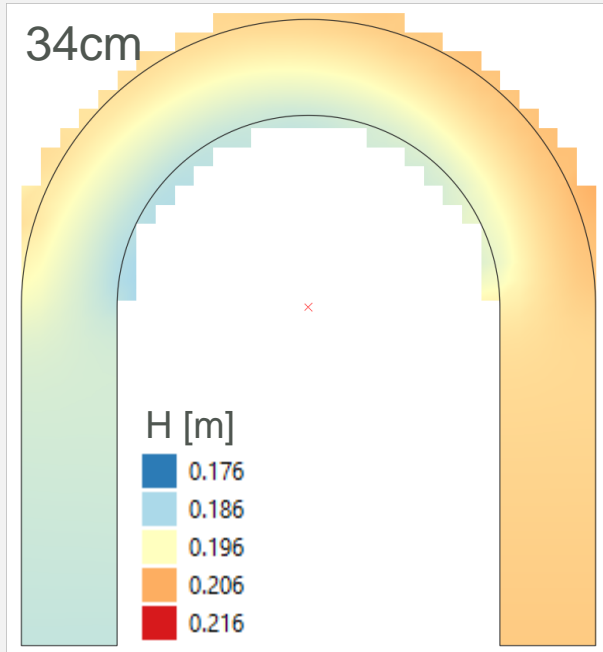
TUFLOW HPC with SGS



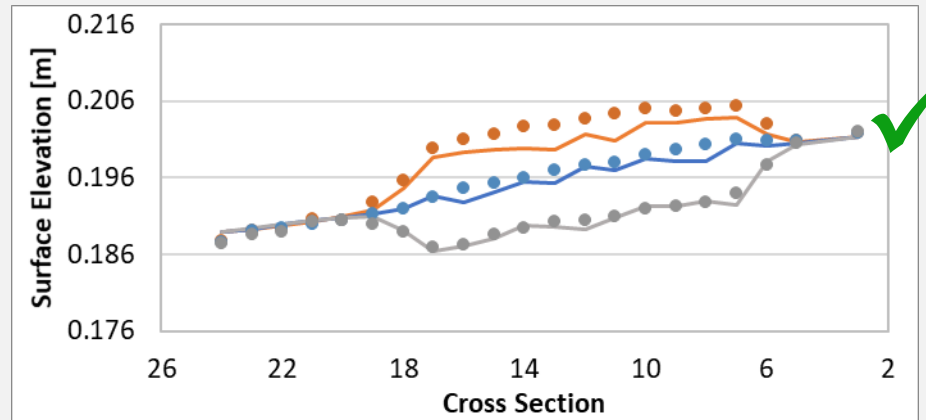
SGS Benchmarking – Cell Size Sensitivity

U-Bend Flume Test – Regular Mesh With SGS

TUFLOW HPC with SGS



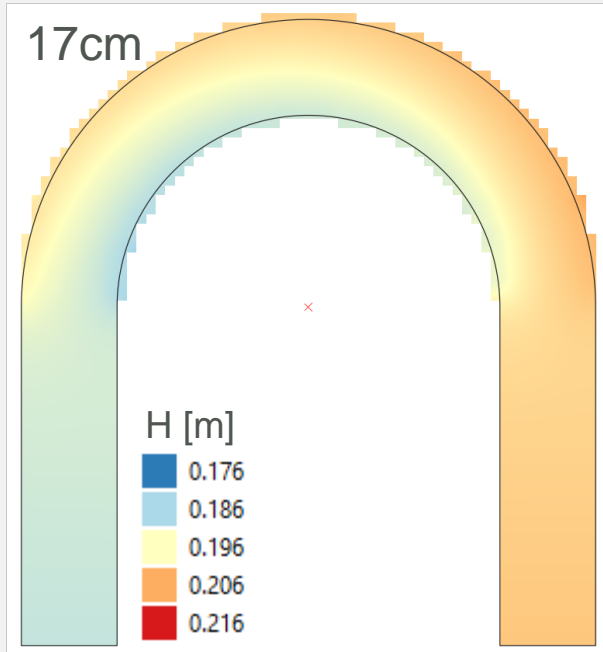
Good agreement with measured upstream water level across wide range of cell sizes 😊



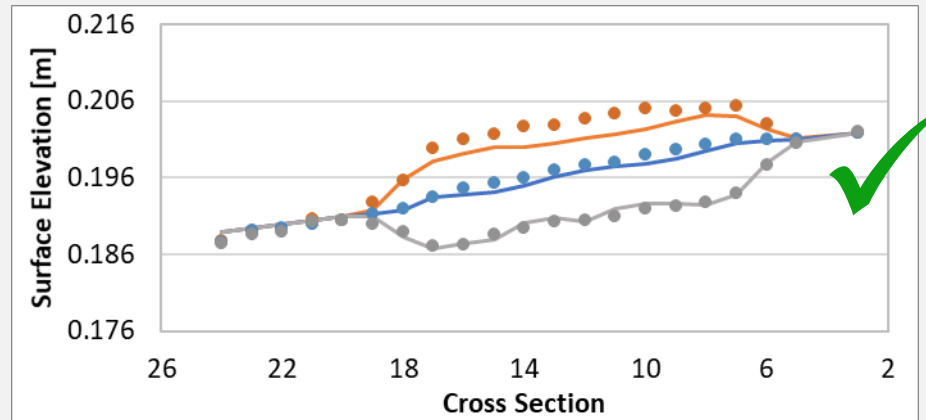
SGS Benchmarking – Cell Size Sensitivity

U-Bend Flume Test – Regular Mesh With SGS

TUFLOW HPC with SGS



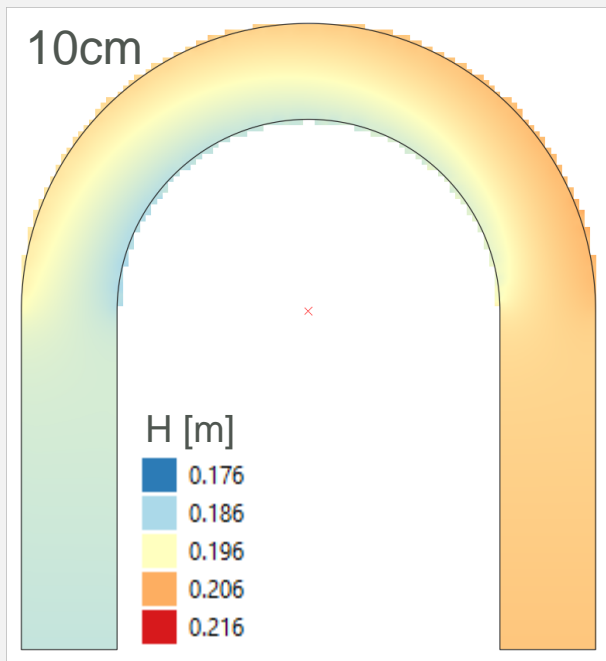
Good agreement with measured upstream water level across wide range of cell sizes 😊



SGS Benchmarking – Cell Size Sensitivity

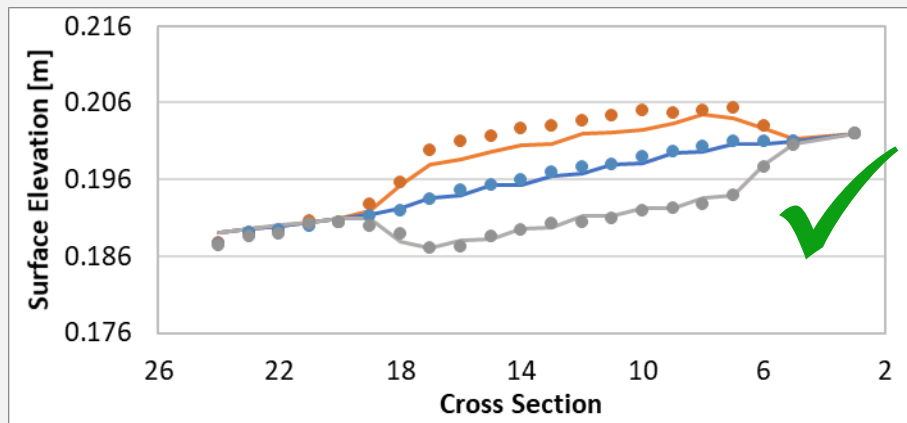
U-Bend Flume Test – Regular Mesh With SGS

TUFLOW HPC with SGS



Good agreement with measured upstream water level across wide range of cell sizes 😊

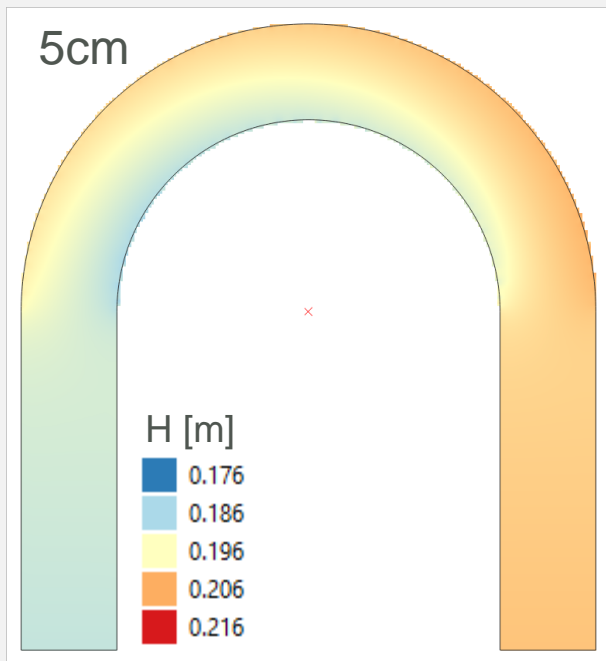
Finer resolutions as good as TUFLOW FV irregular mesh



SGS Benchmarking – Cell Size Sensitivity

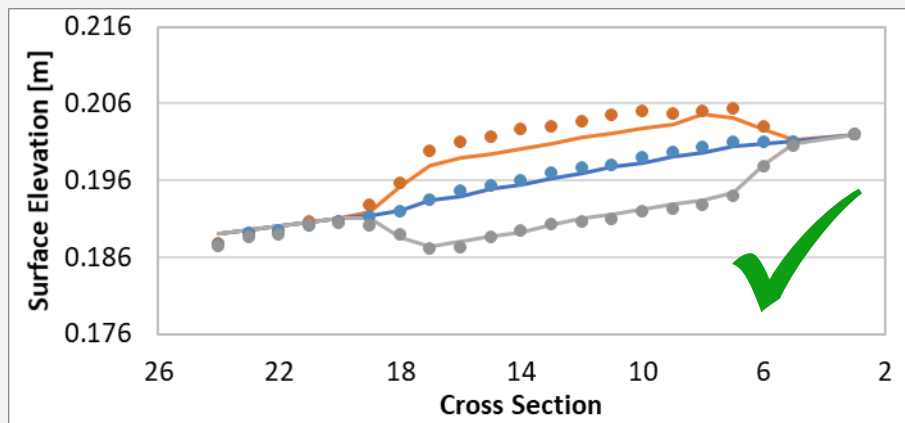
U-Bend Flume Test – Regular Mesh With SGS

TUFLOW HPC with SGS



Good agreement with measured upstream water level across wide range of cell sizes 😊

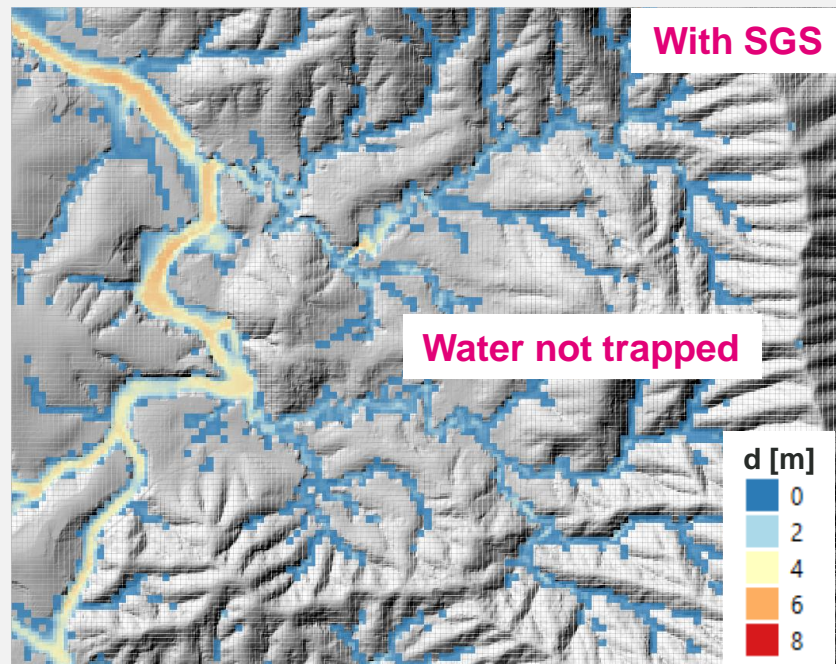
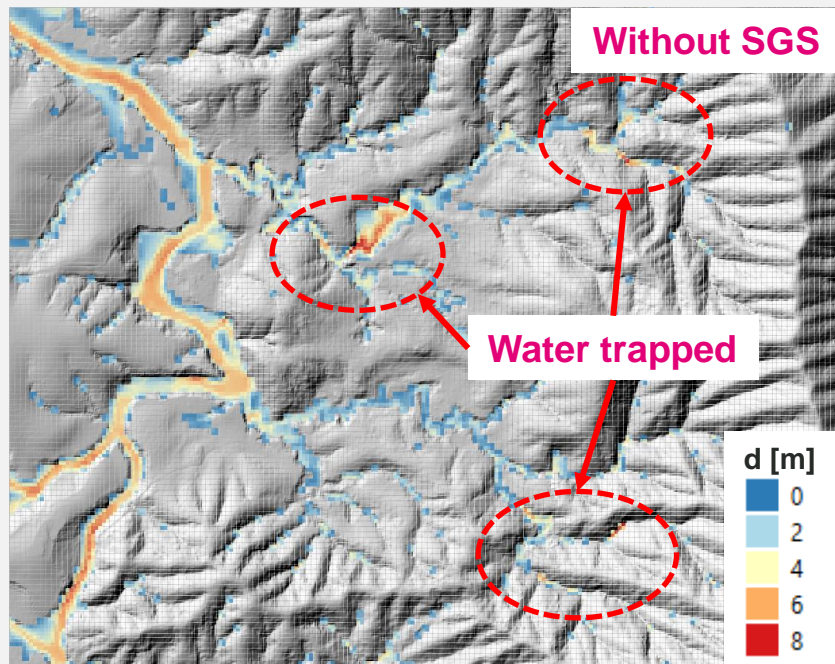
Finer resolutions as good as TUFLOW FV irregular mesh



Direct Rainfall – Whole of Catchment

South Johnstone River Catchment

Effect of having coarse cell sizes

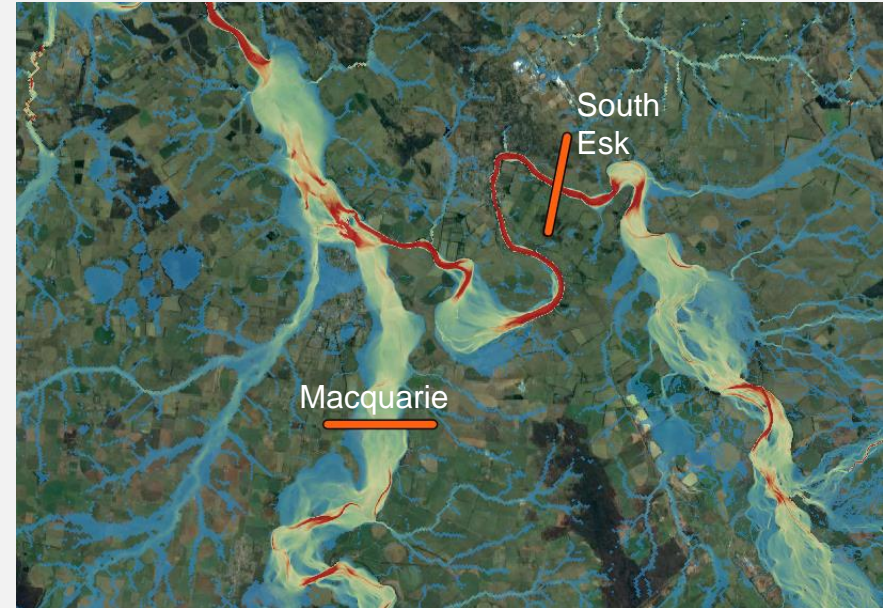
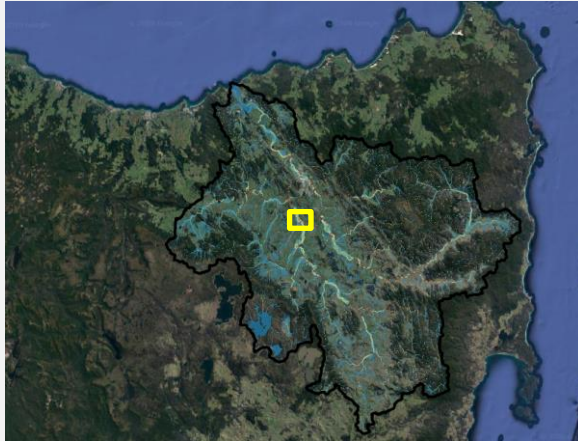


Cell Size Convergence Benchmarking

Tamar River Catchment Model

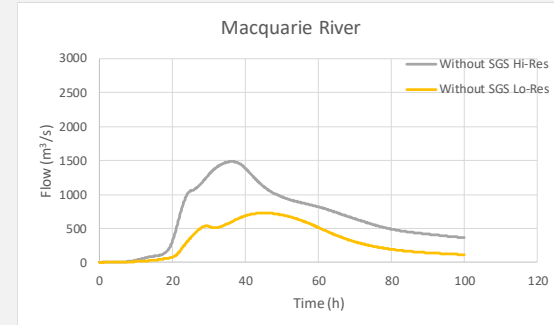
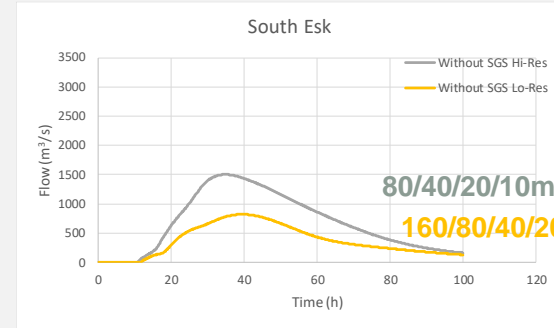
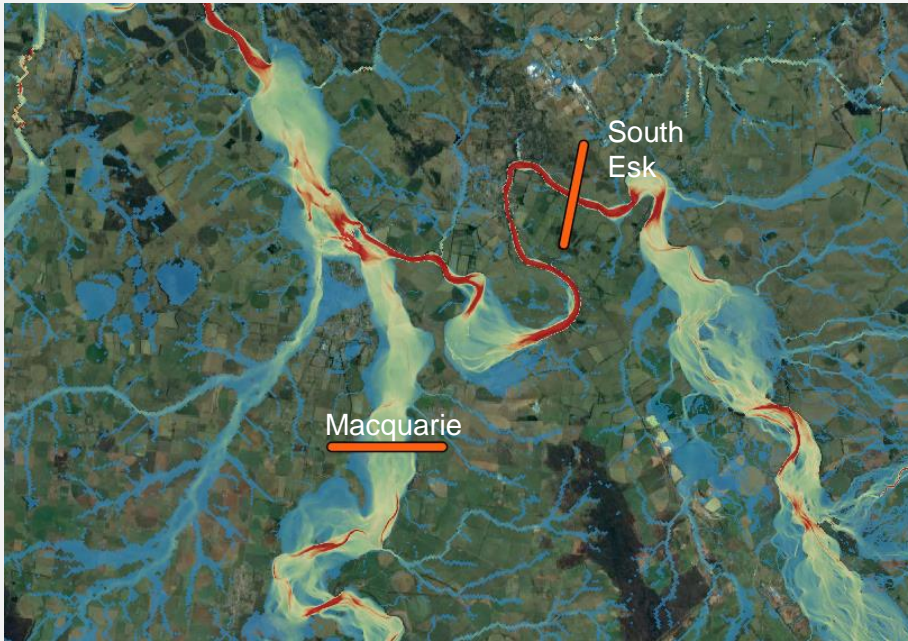
Cell Size Convergence Test

- Do your results (unacceptably) change if you reduce your cell/element sizes?
- A very good test!



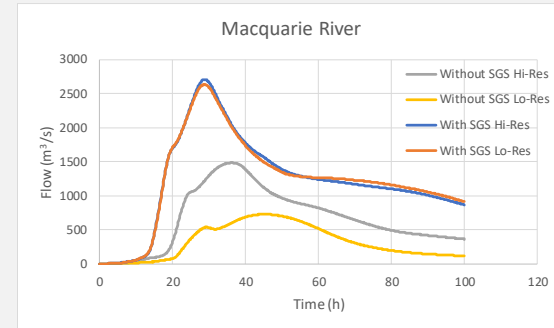
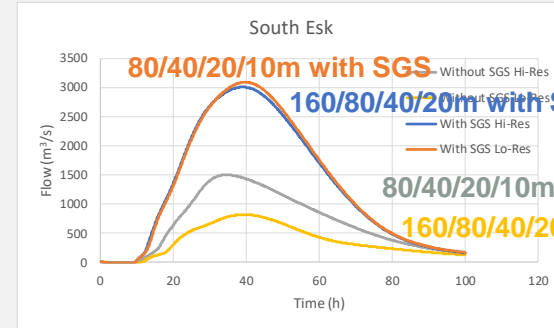
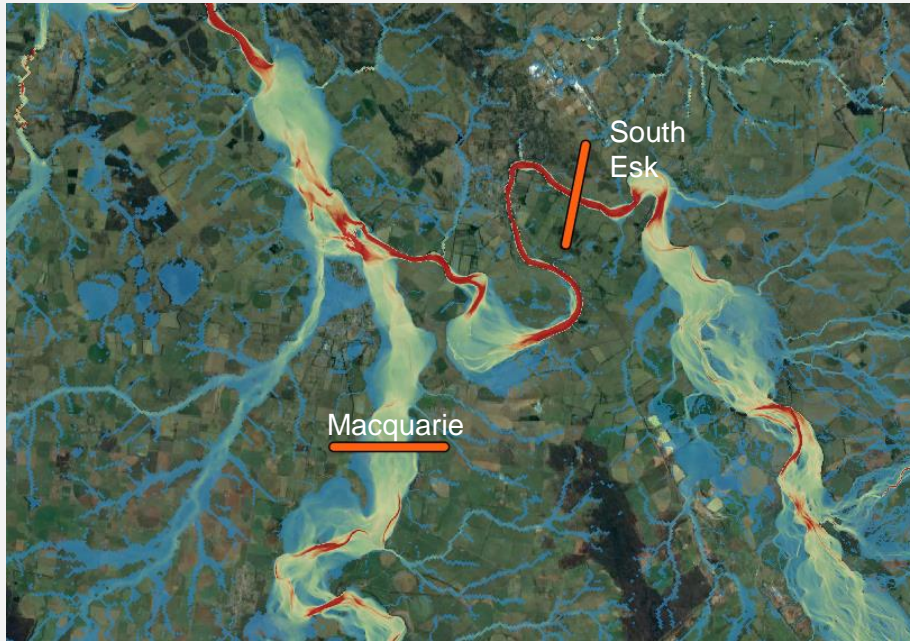
Cell Size Convergence Benchmarking

Tamar River Catchment Model – Without SGS



Cell Size Convergence Benchmarking

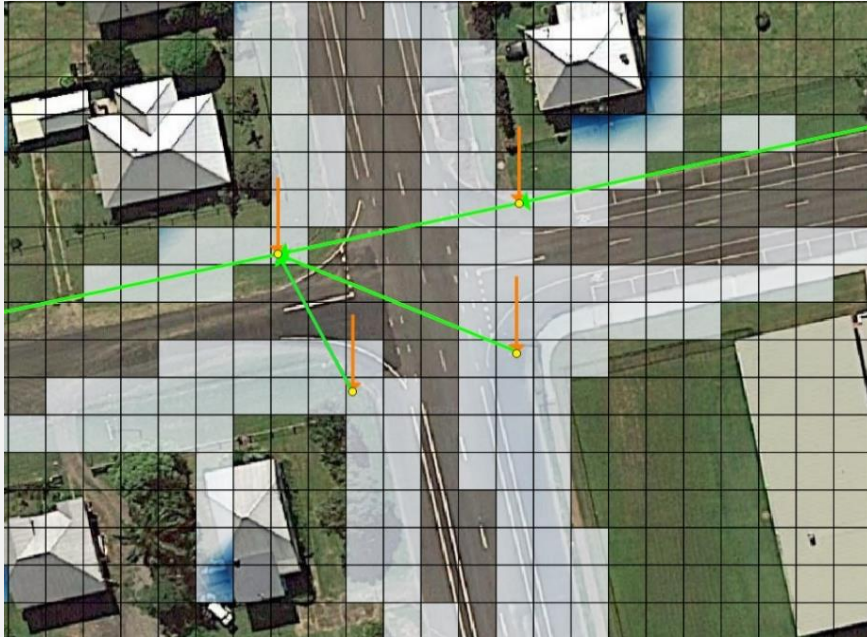
Tamar River Catchment Model – With SGS



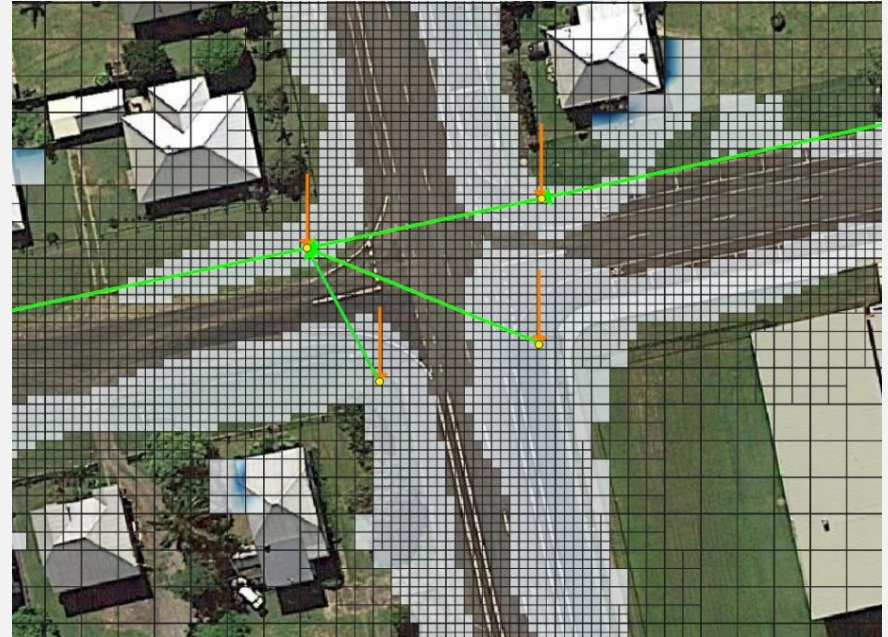
Urban Modelling

Quadtree/SGS Improving Catch-Pit Flow Capture

5 m Single Domain



5m – 2.5m – 1.25m Quadtree Domain

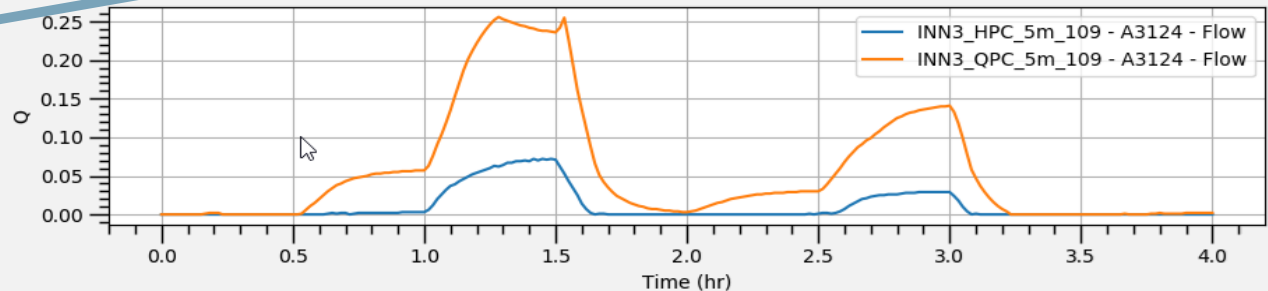
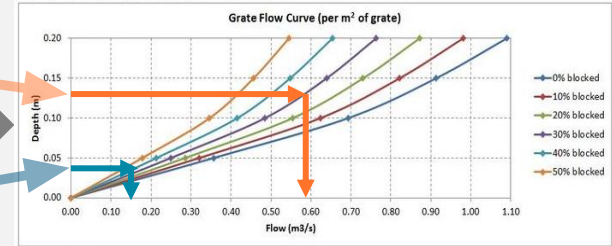
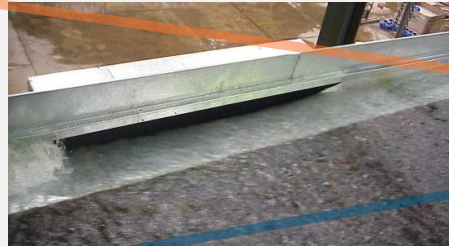
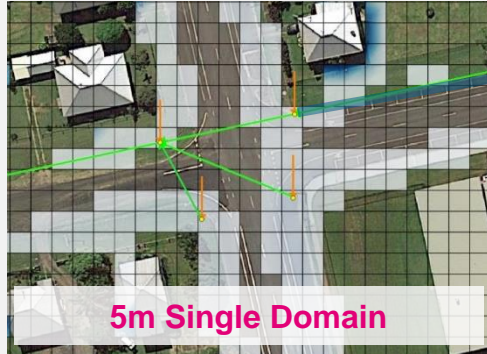


Urban Modelling

Quadtree/SGS Improving Catch-Pit Flow Capture

Improved pit inlet flow capture

- 2D depth at pit inlet more accurate



Conclusion

Three new major features that collectively will benefit all aspects of flood modelling

Cell Size Independent Turbulence Model

- Needed for models using small cells (cell size \ll depth)

Sub-Grid Sampling

- Regular mesh can be rotated at any orientation
- Excellent cell size convergence (carry out preliminary runs at much coarser resolutions)

Quadtree

- Smarter model design
- Excellent mesh creation efficiency

Thank you

